MINNESOTA CONCRETE COUNCIL



WHO IS CRT CONCRETE CONSULTING, LLC?





BACKGROUND OF TULL

- BS in Civil Engineering from Cornell University
- Industry Experience:
 - Concrete Contractor (3 years)
 - Construction Manager (3 years)
 - Ready Mix Concrete (17 years)
- ACI Member
 - 330 Parking Lots
 - 302 Slab Construction
 - 332 Residential Concrete
 - 327 Roller Compacted Concrete
 - 522 Pervious Concrete
- Registered Professional Engineer in Indiana
- LEED AP



SPECIALTY AREAS

- Seminars and Training
- Parking Lot Design
- Concrete Street Design
- Concrete Construction
- Ready Mix Concrete
 - Mix designs
 - Production efficiencies
- Slab on Ground Issues



AGENDA

- Why Concrete Pavements?
- General Information
- Design Theory
- Two Documents
 - ACI 330
 - ACI 325
- Common Items to both 330 and 325
- Parking Lot Design
- Concrete Street Design
- Joints
- Curing



WHY CONCRETE PAVEMENTS?



Why choose concrete over asphalt?







In the past: Truck, Trucks, Trucks



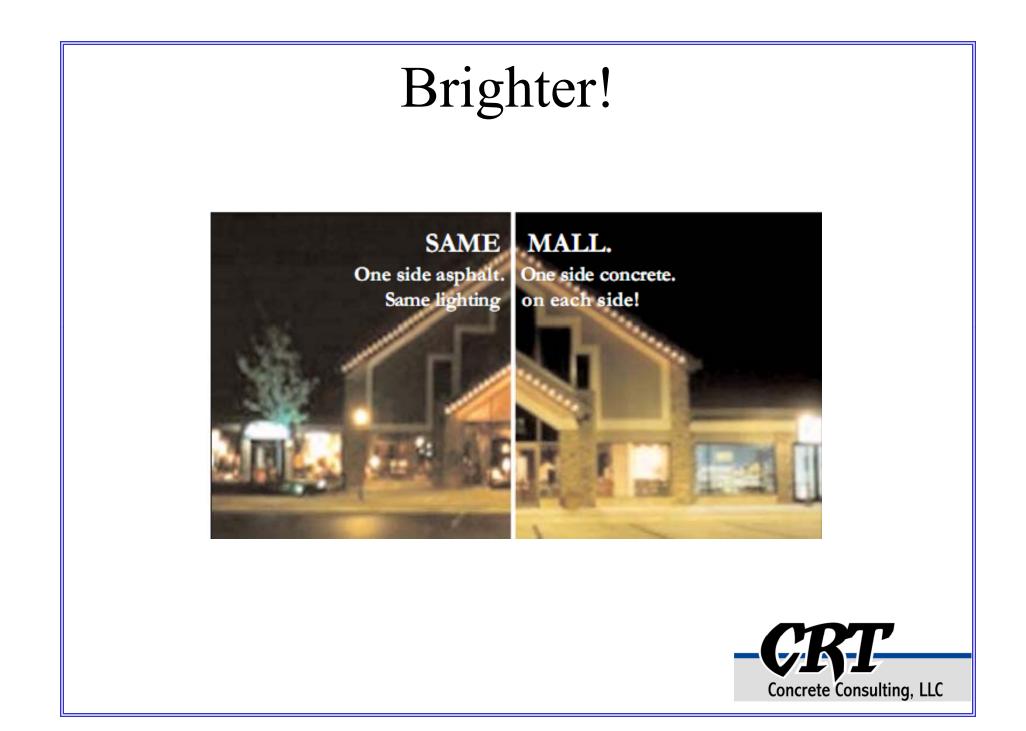
SUSTAINABILITY





LIGHTING AND REFLECTIVITY





Lighting and Reflectivity

- One of the advantages of specifying and designing concrete parking areas is the decrease in the amount of lighting equipment that will be required. The lighter color of concrete reflects more light than a black asphalt area.
- Concrete's reflectivity, or ability to reflect light, provides a marketable benefit over the use of asphalt in parking areas. Studies have shown that concrete parking areas require up to 50% less lighting equipment than a comparable asphalt surface.

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Benefits of Better Lighting:

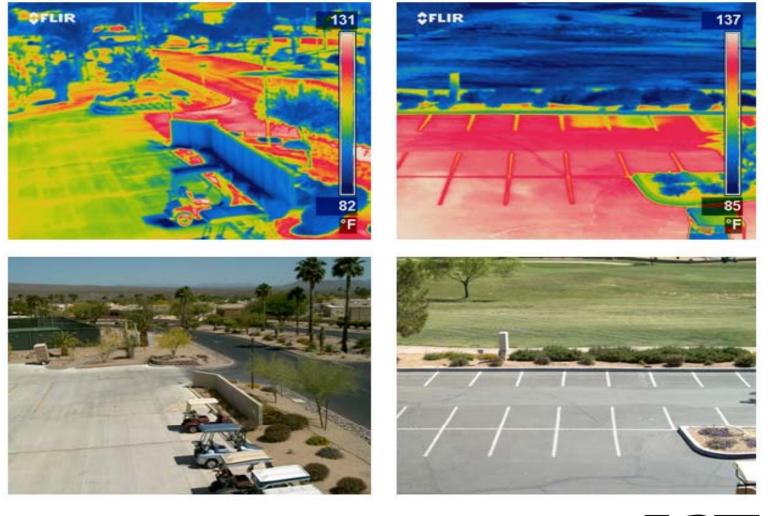
- Savings in initial equipment expense
- Reduced continued energy cost
- A brighter, cleaner parking area
- Increased safety at night
- What types of projects would this benefit the developer?



REDUCED HEAT ISLAND



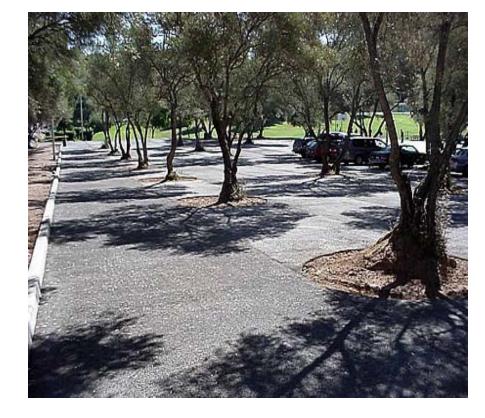
Concrete Pavements Are Cooler

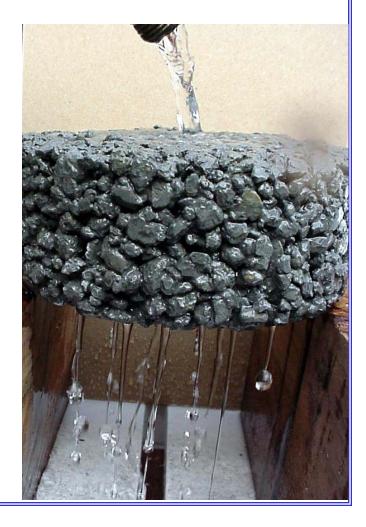


There was a 30-degree difference in temperatures between the asphalt and the concrete surfaces. The photo or the top right was taken of an asphalt parking lot adjacent to a golf course. Note the 85-90 degree temperature of the grass and the 135 degree temperature of the asphalt; the photo below it represents the same scene.

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Pervious Concrete







LITTLE OR NO MAINTENANCE



Low Maintenance





No Dependence of Oil

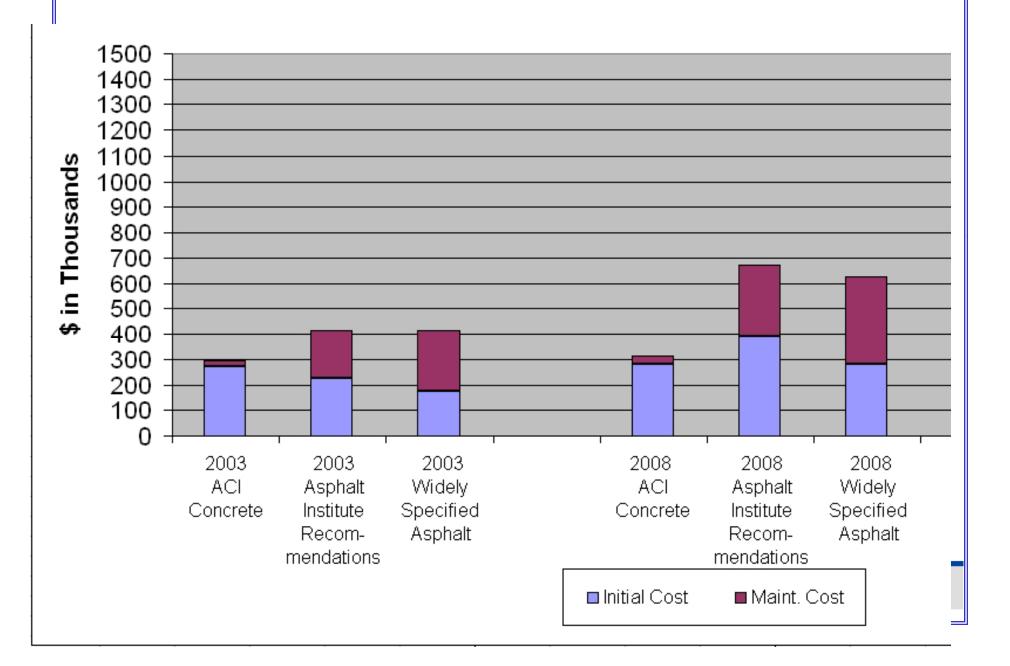


WHAT'S CHANGED TODAY?

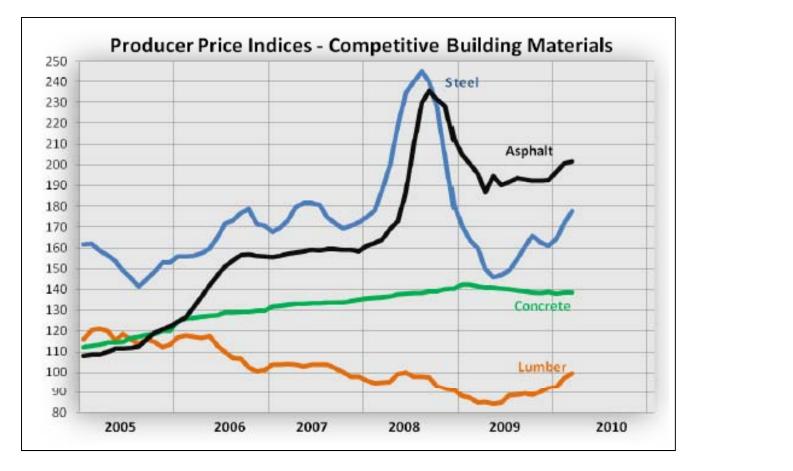
COMPETITIVE UP FRONT COSTS



Economical

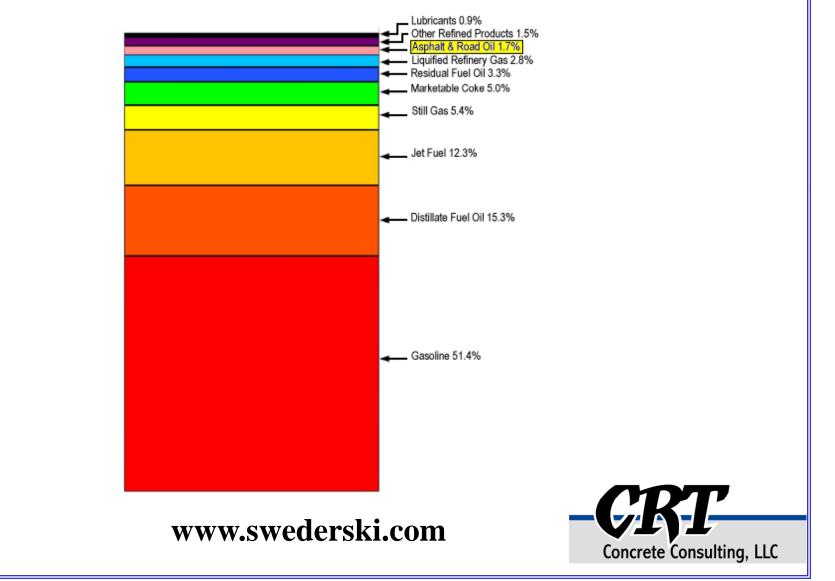


Producer Price Indices Competitive Building Materials





Barrel of Oil Breakdown.



The Trends are Positive

In a world where customers care more and more about the environment and always care about price:

- Concrete costs less.
- Concrete increasingly recognized as "green"
- Asphalt increasingly recognized as having environmental problems
- Asphalt increasingly expensive and unstable.

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Concrete, today enjoys a position never before experienced by our industry



CONCRETE PAVEMENTS: GENERAL INFORMATION



Jointed - unreinforced (plain) pavement

Plan



Profile





Jointed & Doweled Pavement

Plan



Profile





Jointed - reinforced pavement

Plan



Profile

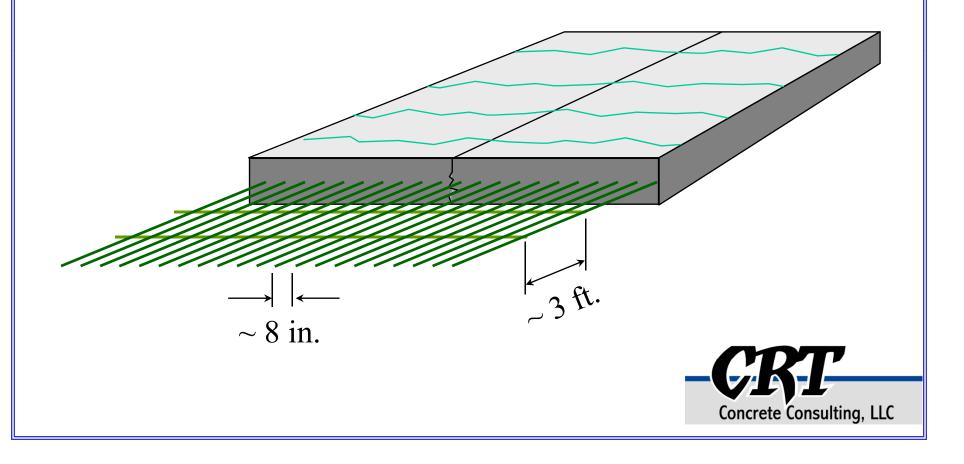


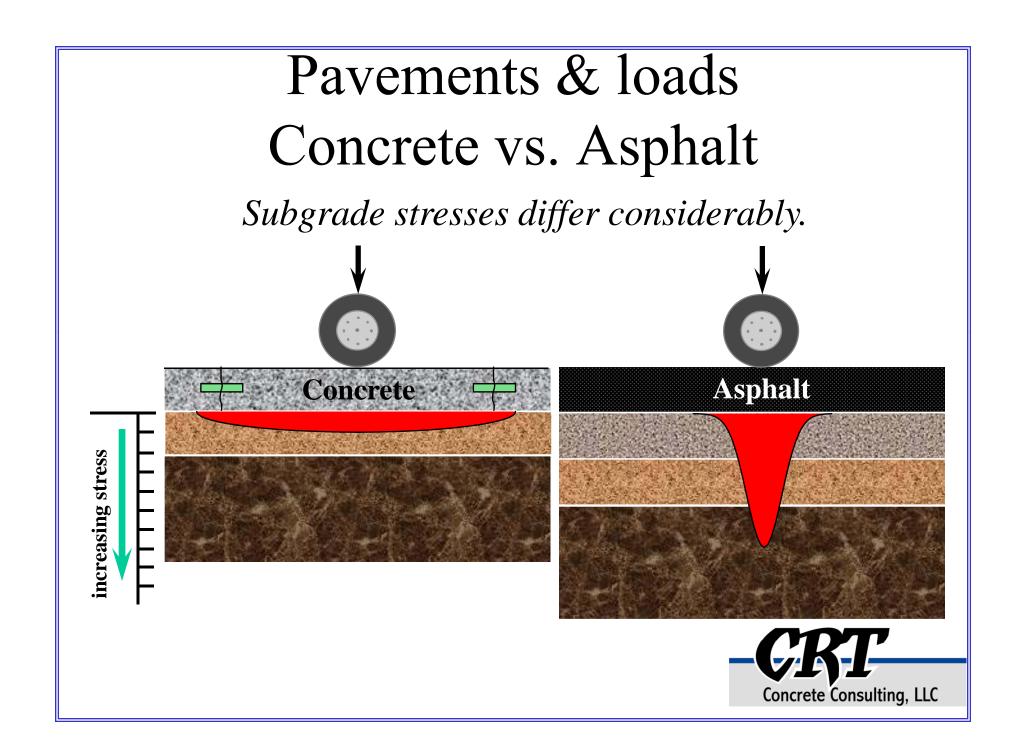
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Distributed steel reinforcement is used to prevent the opening of expected random cracks between joints

Continuously reinforced concrete (CRC) pavement

- Heavily reinforced without joints
- Stable transverse cracks develop every 3-6 feet.





DESIGN THEORY



Pavement Engineering

Pavement engineering is the art of molding materials we do not wholly understand into shapes we cannot precisely analyze, so as to withstand forces we cannot assess, in such a way that the community at large has no reason to suspect our ignorance.



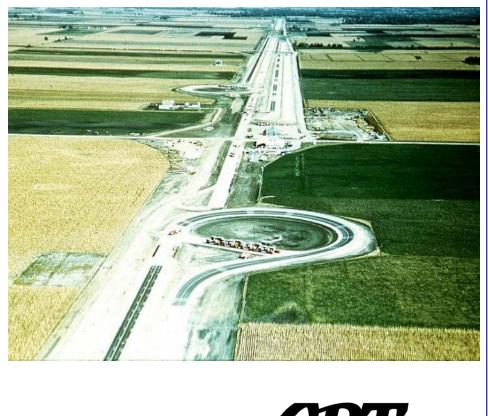
Thickness Design Procedures

- Empirical Design
 - Based on observed performance
 - AASHO Road Test
- Mechanistic Design
 - Based calculated pavement responses
 - PCA Design Procedure (PCAPAV)
 - StreetPave (ACPA Design Method)
 - ACI 330 Design Tables
 - ACI 325 Design Tables

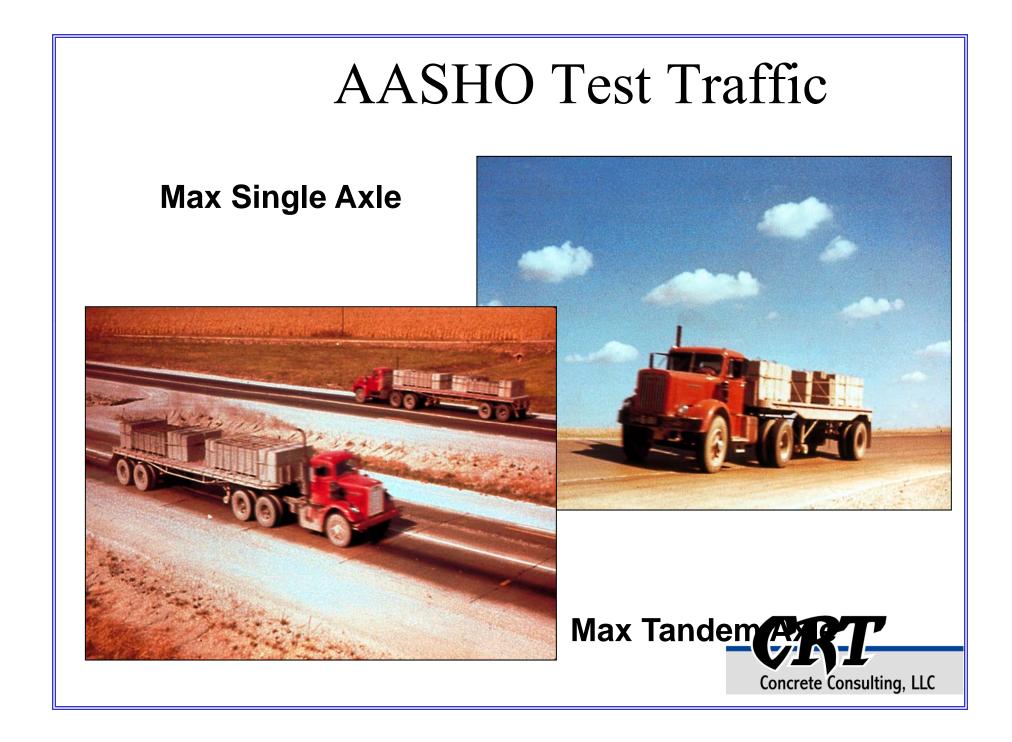


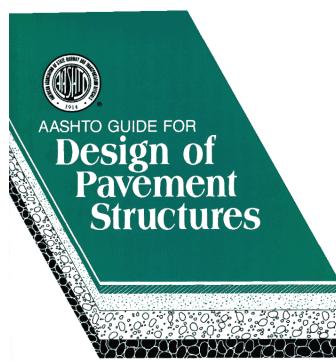
Source of Much of What We Know About Pavement Design

- AASHO Road Test
- Late 50's and early 60's
- Ottawa, Illinois



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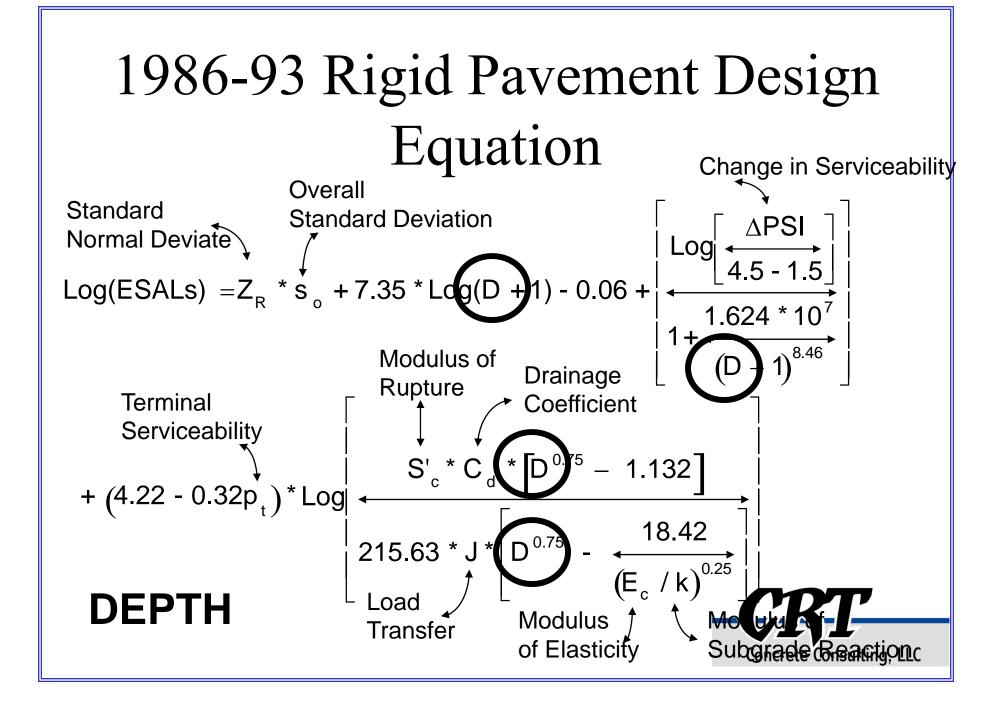


PUBLISHED BY THE AMERICAN ASSOCIATION OF STATE HIGHWAY AND TRANSPORTATION OFFICIALS

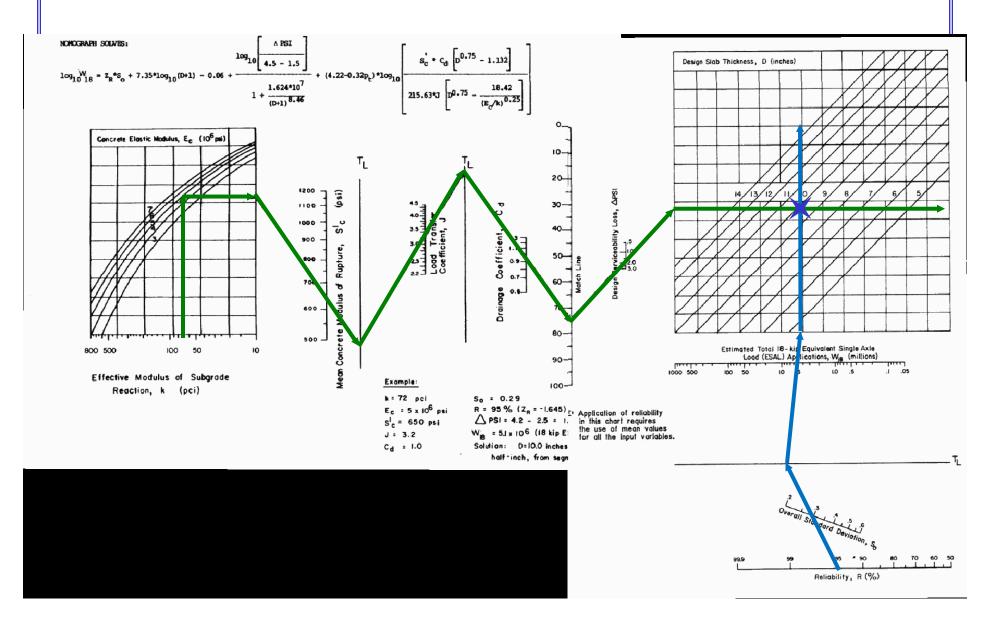
AASHTO '93 Guide

- Pavements Can be Compared at Roughly Equivalent Levels of Reliability
- Principles in both versions are identical for new construction





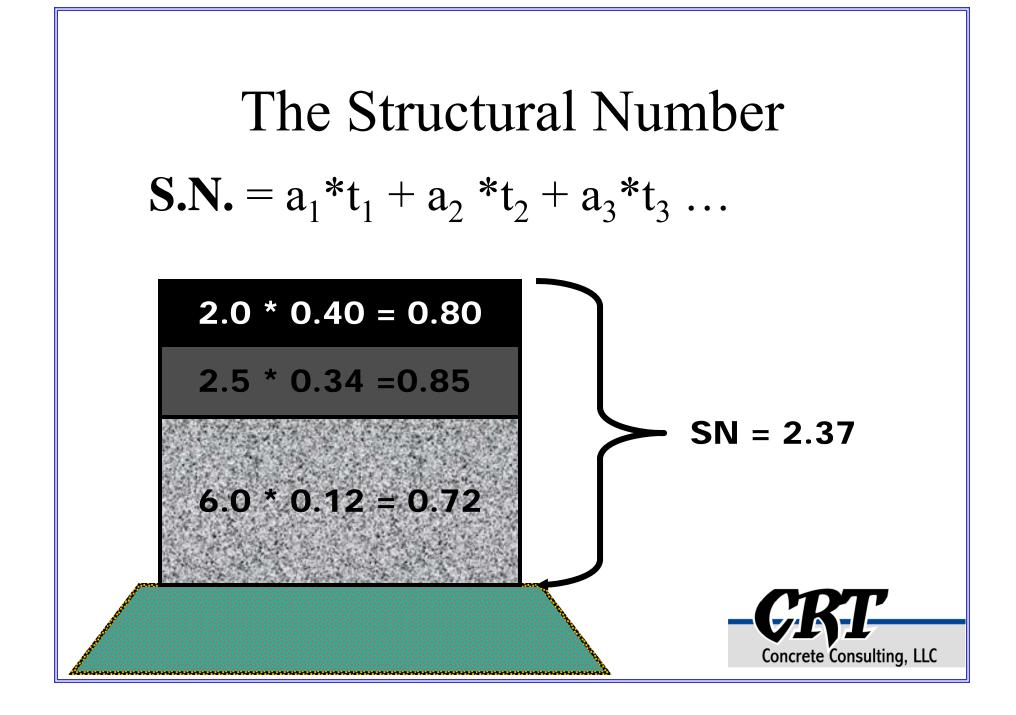
Rigid Design Nomograph



What About Concrete Structural Coefficients?

- Based on Louisiana AASHO satellite studies
- Used principally for overlay design
- Value set at 0.50 for old concrete
- Calculations from the AASHTO equations incorporating reliability concepts for new pavement show a minimum value of 0.47 to 0.74 depending on strength for plain pavement





Bituminous Structural Coefficients

Source: Chapter 54, IL D.O.T. Design Manual, 2000

STRUCTURAL MATERIALS		IUM STRE QUIREME		COEFFICIENTS ³			
	MS [®]	IBR	CS©	21	a2	a 3	
	Bitumin	ious Surfac	e				
Road Mix (Class B)				0.20			
Plant Mix (Class B)							
Liquid Asphalt				0.22			
Asphalt Cement	900			0.30			
Class I Bituminous Concrete	1700			0.40			
	Base	e Course					
Aggregate, Type B Uncrushed							
Uncrushed		50			0.10		
Crushed		80			0.13		
Aggregate, Type A		80			0.13		
Waterbound Macadam		110			0.14		
Bituminous Stabilized Granular Material	300				0.16		
	400				0.18		
	800				0.23		
	1000				0.25		
	1200				0.27		
	1500				0.30		
	1700				0.33		
Class I Binder	1700				0.33		
Pozzolanic, Type A			600		0.28		
Lime Stabilized Soil			150		0.11		
Select Soil Stabilized			300		0.15		
with Cement			500		0.20		
Cement Stabilized Granular							
Material			650		0.23		
			750		0.25		
			1000		0.28		
	Su	ibbase			·		
Granular Material, Type B Granular Material, Type A		30				0.1	
Uncrushed		50				0.12	
Crushed		80				0.14	
Lime Stabilized Soil			100			0.12	

Notes:

- Marshall Stability (MS) index or equivalent.
- Compressive strength (CS) in pounds per square inch (psi). For cement stabilized soils and granular materials, use the 7-day compressive strength that can be reasonably expected under field conditions. For lime stabilized soils, use the accelerated curing compressive strength at 120°F for 48 hours. For Pozzolanic, Type A, use the compressive strength after a 14-day curing period at 72°F.
- In For materials with strengths other than those shown, the coefficients may be determined from Figures 54-50, 54-5P, and 54-5Q. Other approved materials of similar strengths may be substituted for those presented in Figure 54-5N.

COEFFICIENTS FOR MATERIALS IN NEW FLEXIBLE PAVEMENT STRUCTURES

AASHTO '93 Local Roads Catalog Designs

 Table 4.7.
 Flexible Pavement Design Catalog for Low-Volume Roads: Recommended Ranges of Structural Number (SN) for Six U.S. Climatic Regions. Three Levels of Axle Load Traffic and Five Levels of Roadbed Soil Quality

Traffic	U.S. limatic Region								
Level	Ι	II	l)	IV	V	VI			
High Medium	2.6–2.7* 2.3–2.5	2.8–2.9 2.5–2.7	3.0-3.2 2.7-3.0	2.4–2.5 2.1–2.3	2.7-2.8	3.0-3.2 2.7-3.0			
Low	1.6-2.1	1.8-2.3	2.0-2.6	1.5-2.0	1.7–2.2	2.0-2.6			
High Medium Low	2.9-3.0 2.6-2.8 1.9-2.4	3.0-3.2 2.7-3.0 2.0-2.6	3.3-3.4 3.0-3.2 2.2-2.8	2.7-2.8 2.4-2.6 1.8-2.3	3.0-3.1 2.6-2.9 2.0-2.5	3.3-3.4 2.9-3.2 2.2-2.8			
High Medium Low	3.2-3.3 2.8-3.1 2.1-2.7	3.3-3.4 2.9-3.2 2.2-2.8	3.4-3.5 2.7-3.3 2.3-2.9	Say	2.1-2.7	3.4–3.5 3.0–3.3 2.3–2.9			
High Medium ≻ Low	3.5-3.6 3.1-3.4 2.4-3.0	3.6-3.7 3.2-3.5 2.4-3.0	3.7-3.9 3.4-3.6 2.5-3.2	3.4-3.5 3.0-3.3 2.3-2.8	3.5-3.6 3.1-3.4	3.7-3.8 3.3-3.6 2.5-3.2			
High Medium Low	3.8-3.9 3.4-3.7 2.6-3.2	3.8-4.0 3.5-3.8 2.5-3.3	3.8-4.0 3.5-3.7 2.6-3.3	3.6-3.8 3.3-3.6 2.5-3.1	3.7-3.8 3.3-3.6	3.8-4.0			
•	High Medium Low High Medium Low High Medium Low High Medium Low High Medium	LevelIHigh2.6-2.7*Medium2.3-2.5Low1.6-2.1High2.9-3.0Medium2.6-2.8Low1.9-2.4High3.2-3.3Medium2.8-3.1Low2.1-2.7High3.5-3.6Medium3.1-3.4Low2.4-3.0High3.8-3.9Medium3.4-3.7	LevelIIIHigh $2.6-2.7*$ $2.8-2.9$ Medium $2.3-2.5$ $2.5-2.7$ Low $1.6-2.1$ $1.8-2.3$ High $2.9-3.0$ $3.0-3.2$ Medium $2.6-2.8$ $2.7-3.0$ Low $1.9-2.4$ $2.0-2.6$ High $3.2-3.3$ $3.3-3.4$ Medium $2.8-3.1$ $2.9-3.2$ Low $2.1-2.7$ $2.2-2.8$ High $3.5-3.6$ $3.6-3.7$ Medium $3.1-3.4$ $3.2-3.5$ Low $2.4-3.0$ $2.4-3.0$ High $3.8-3.9$ $3.8-4.0$ Medium $3.4-3.7$ $3.5-3.8$	HameIIIIIHigh $2.6-2.7*$ $2.8-2.9$ $3.0-3.2$ Medium $2.3-2.5$ $2.5-2.7$ $2.7-3.0$ Low $1.6-2.1$ $1.8-2.3$ $2.0-2.6$ High $2.9-3.0$ $3.0-3.2$ $3.3-3.4$ Medium $2.6-2.8$ $2.7-3.0$ $3.0-3.2$ Low $1.9-2.4$ $2.0-2.6$ $2.2-2.8$ High $3.2-3.3$ $3.3-3.4$ $3.4-3.5$ Medium $2.8-3.1$ $2.9-3.2$ $2.7-3.3$ Low $2.1-2.7$ $2.2-2.8$ $2.3-2.9$ High $3.5-3.6$ $3.6-3.7$ $3.7-3.9$ Medium $3.1-3.4$ $3.2-3.5$ $3.4-3.6$ Low $2.4-3.0$ $2.4-3.0$ $2.5-3.2$ High $3.8-3.9$ $3.8-4.0$ $3.8-4.0$ Medium $3.4-3.7$ $3.5-3.8$ $3.5-3.7$	ItaliteIIIIMIVHigh $2.6-2.7*$ $2.8-2.9$ $3.0-3.2$ $2.4-2.5$ Medium $2.3-2.5$ $2.5-2.7$ $2.7-3.0$ $2.1-2.3$ Low $1.6-2.1$ $1.8-2.3$ $2.0-2.6$ $1.5-2.0$ High $2.9-3.0$ $3.0-3.2$ $3.3-3.4$ $2.7-2.8$ Medium $2.6-2.8$ $2.7-3.0$ $3.0-3.2$ $2.4-2.6$ Low $1.9-2.4$ $2.0-2.6$ $2.2-2.8$ $1.8-2.3$ High $3.2-3.3$ $3.3-3.4$ $3.4-3.5$ SayMedium $2.8-3.1$ $2.9-3.2$ $2.7-3.3$ SayLow $2.1-2.7$ $2.2-2.8$ $2.3-2.9$ 2.6 High $3.5-3.6$ $3.6-3.7$ $3.7-3.9$ $3.4-3.5$ Medium $3.1-3.4$ $3.2-3.5$ $3.4-3.6$ $3.0-3.3$ Low $2.4-3.0$ $2.4-3.0$ $2.5-3.2$ $2.3-2.8$ High $3.8-3.9$ $3.8-4.0$ $3.8-4.0$ $3.6-3.8$ Medium $3.4-3.7$ $3.5-3.8$ $3.5-3.7$ $3.3-3.6$	ItaliteIIIIVVHigh $2.6-2.7^*$ $2.8-2.9$ $3.0-3.2$ $2.4-2.5$ $2.7-2.8$ Medium $2.3-2.5$ $2.5-2.7$ $2.7-3.0$ $2.1-2.3$ $2.4-2.6$ Low $1.6-2.1$ $1.8-2.3$ $2.0-2.6$ $1.5-2.0$ $1.7-2.2$ High $2.9-3.0$ $3.0-3.2$ $3.3-3.4$ $2.7-2.8$ $3.0-3.1$ Medium $2.6-2.8$ $2.7-3.0$ $3.0-3.2$ $2.4-2.6$ $2.6-2.9$ Low $1.9-2.4$ $2.0-2.6$ $2.2-2.8$ $1.8-2.3$ $2.0-2.5$ High $3.2-3.3$ $3.3-3.4$ $3.4-3.5$ Say 2.9Low $2.1-2.7$ $2.2-2.8$ $2.3-2.9$ 2.6 $2.1-2.7$ High $3.5-3.6$ $3.6-3.7$ $3.7-3.9$ $3.4-3.5$ $3.0-3.3$ Low $2.4-3.0$ $2.4-3.0$ $2.5-3.2$ $2.3-2.8$ $2.3-2.9$ High $3.8-3.9$ $3.8-4.0$ $3.8-4.0$ $3.6-3.8$ $3.7-3.8$ Medium $3.4-3.7$ $3.5-3.8$ $3.5-3.7$ $3.3-3.6$ $3.3-3.6$			

Concrete Co

Let's Build an Asphalt Section

1.5" Bit. SC x 0.40 = 0.80

1.5" Binder x 0.33 = 0.50

6" Crushed Stone x 0.14 = 0.84

7" Type B Granular x 0.11 = 0.77

SN = 0.8 + 0.5 + 0.84 + 0.77 = 2.91

Concrete Consulting, LLC

AASHTO '93 Local Roads Catalog Designs

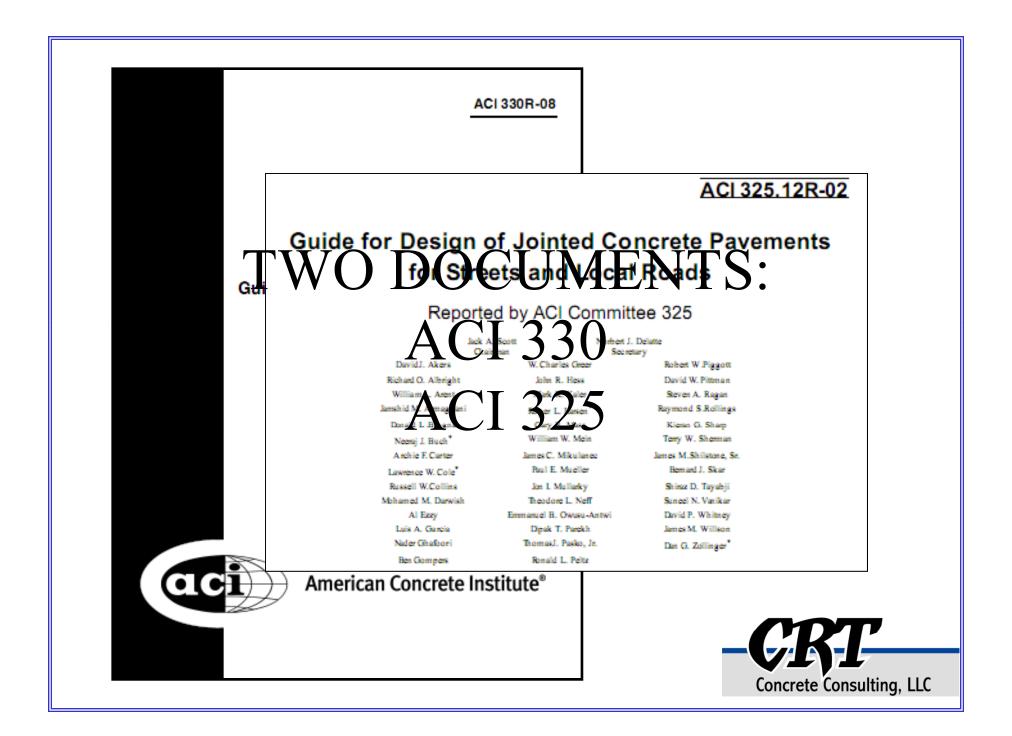
Low-Volume Road Design

II-85

PUBLISHED BY THE W ASSOCIATION OF STATE HIGHWAY AND TRANSPORT

Table 4.9(b).Rigid Design Catalog for Low-Volume Roads: Recommended Minimum PCC Slab
Thickness (Inches) for Three Levels of Axle Load Traffic and Five Levels of Roadbed
Soil Quality

			nt reliability Franular Sut	7: 75 percent.					
oad Transfer Devices		Ň	0			Y	/es		
Edge Support	N	lo	Y	es	No		Y	es	
S' _c (psi)	600	700	600	700	600	700	600	700	
Relative Quality of Roadbed Soil				affic					
Very good & good	5.5	5	5	5	5	5	5	5	
Fair	5.75	5.25	5	5	5	5	5	5	
Poor & very poor	5.75	5.25	5	5	5	5	5	5	
				Medium '	Traffic				
Very good & good	6.25	5.75	5.75	5.25	6	5.5	5.5	5	
Fair	6.5	5.75	6	5.5	6.25	5.5	5.5	5	
Poor & very poor	6.5	6	6	5.5	6.25	5.75	5. *	5.75	
	High Traffic								
Very good & good	7.25	6.5	6.5	6	6.75	6	6 ^D	esign of Pavemen	
Fair	7.25	6.5	6.5	6	6.75	6	6	Structur	
Poor & very poor	7.25	6.75	6.75	6	6.75	6.25	6.1		



COMMON ITEMS IN ACI 330 AND ACI 325



Common Items:

- Pavement Stresses
- Subbase Support
- Concrete Properties
- Secondary Reinforcement

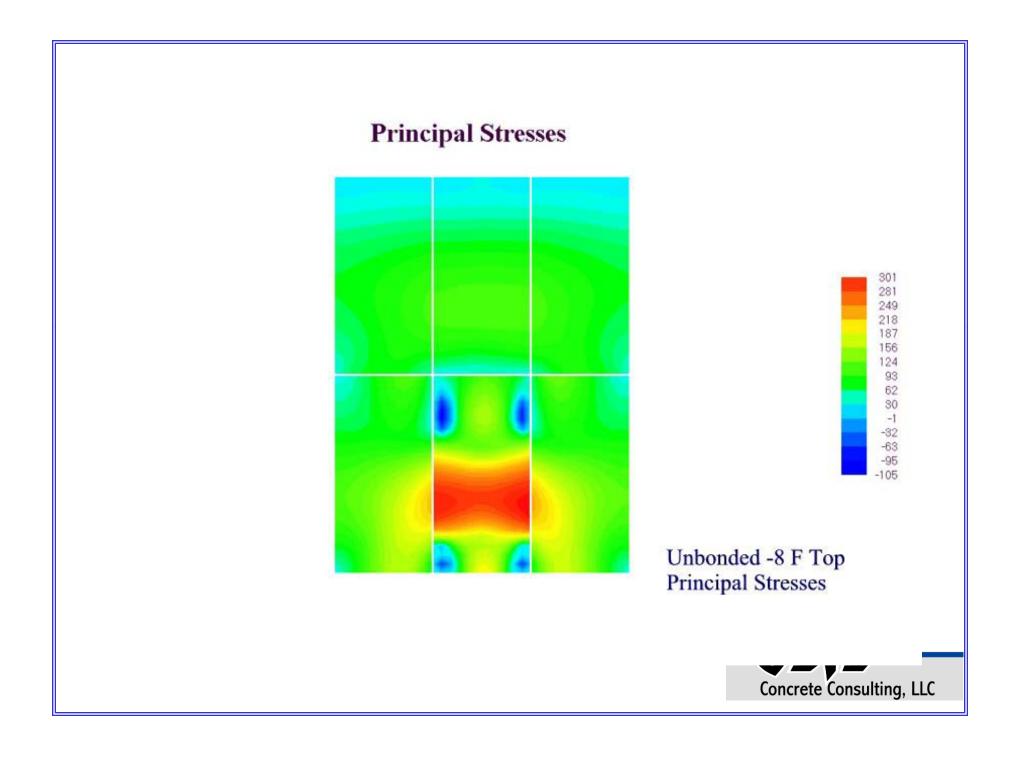


3.2 Pavement Stresses

- Higher when wheels are at or near an unsupported edge.
- Highest stresses
 occurs at the
 intersection of a
 joint and an
 unsupported edge

Thickness design of pavement is intended to limit slab tensile stresses produced by vehicular loading. Model studies, as well as full-scale accelerated traffic tests, have shown that maximum tensile stresses in concrete pavement occur when vehicle wheels are close to a free or unsupported edge of the pavement. Stresses resulting from wheel loadings applied near interior joints are generally less severe due to load transfer across the joints. The critical stress condition occurs when a wheel load is applied near the intersection of a joint and the pavement edge. Because parking areas have relatively little area adjacent to free edges and vehicle loads are applied mostly to interior slabs, pavements should be designed assuming supported edges. At the outside edges or at entrances, integral curbs or thickened edge sections can be used to decrease stresses. Thermal expansion and contraction of the pavement and warping or curling caused by moisture and temperature differentials within the pavement cause other stresses that are not addressed directly in thickness design. Proper jointing reduces these stresses.





CONCRETE PROPERTIES



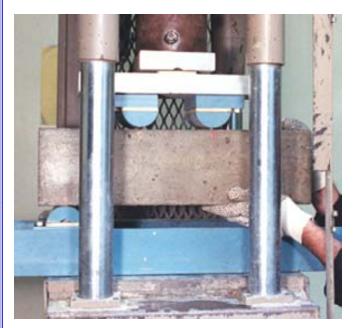
Concrete materials



- Strength
 - Consistent with design
 - More is not necessarily better
- Durability
 - Entrained air for freeze/thaw
 - Sulfates, AAR considerations if applicable
- Other performance requirements
 - Economy
 - Workability
 - Lowest shrinkage potential
 - Water content, slump
 - Aggregate size & grading



Concrete strength



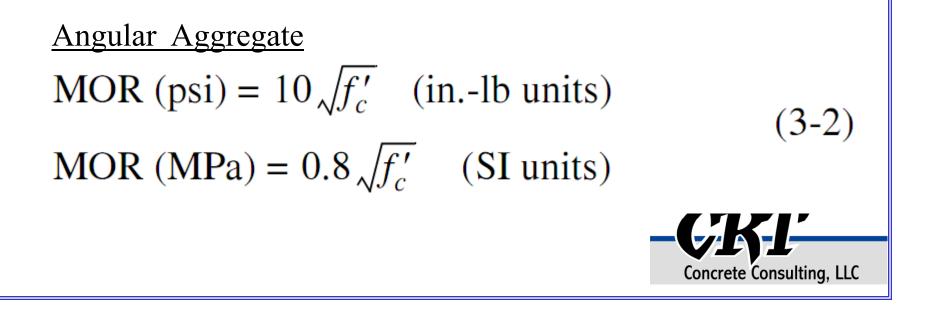
While compressive strength (f'_c) is specified and used for quality control on most projects, modulus of rupture (M_R) is used for thickness design. The M_R of a concrete mix may be estimated using typical relationships ($M_R \approx 8$ to 10 x $\sqrt{}$ f'_c) or actual data from tests using proposed materials.



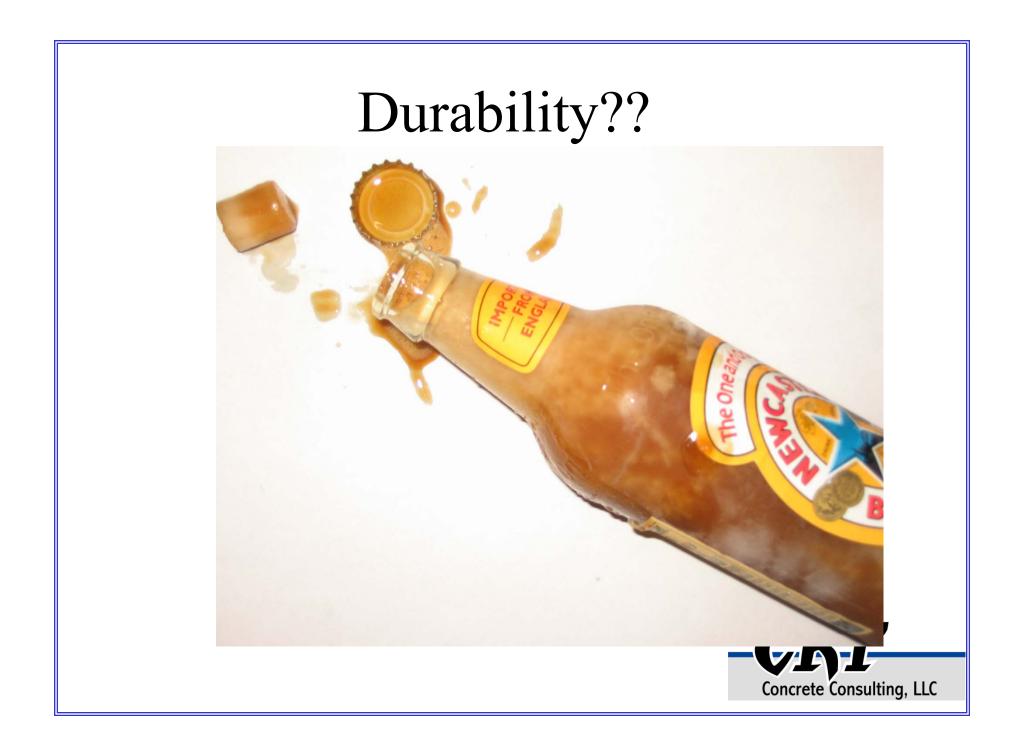


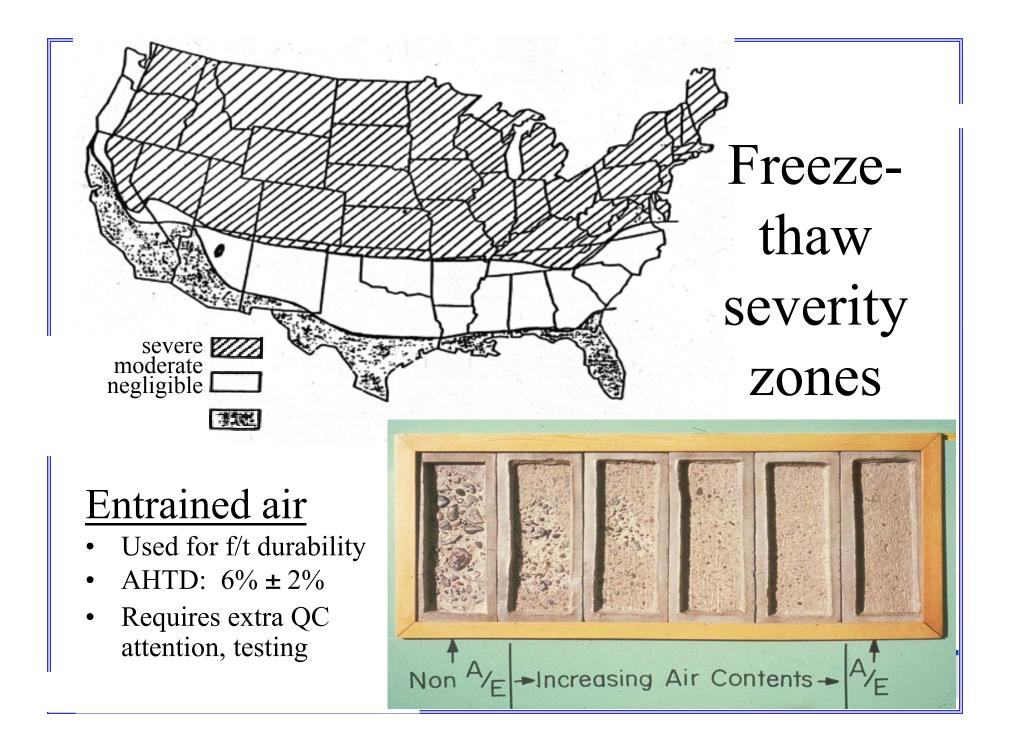
M_R estimation, (pg 6, ACI 330R) <u>Round Aggregate</u>

MOR (psi) = $8\sqrt{f'_c}$ (in.-lb units) MOR (MPa) = $0.7\sqrt{f'_c}$ (SI units)



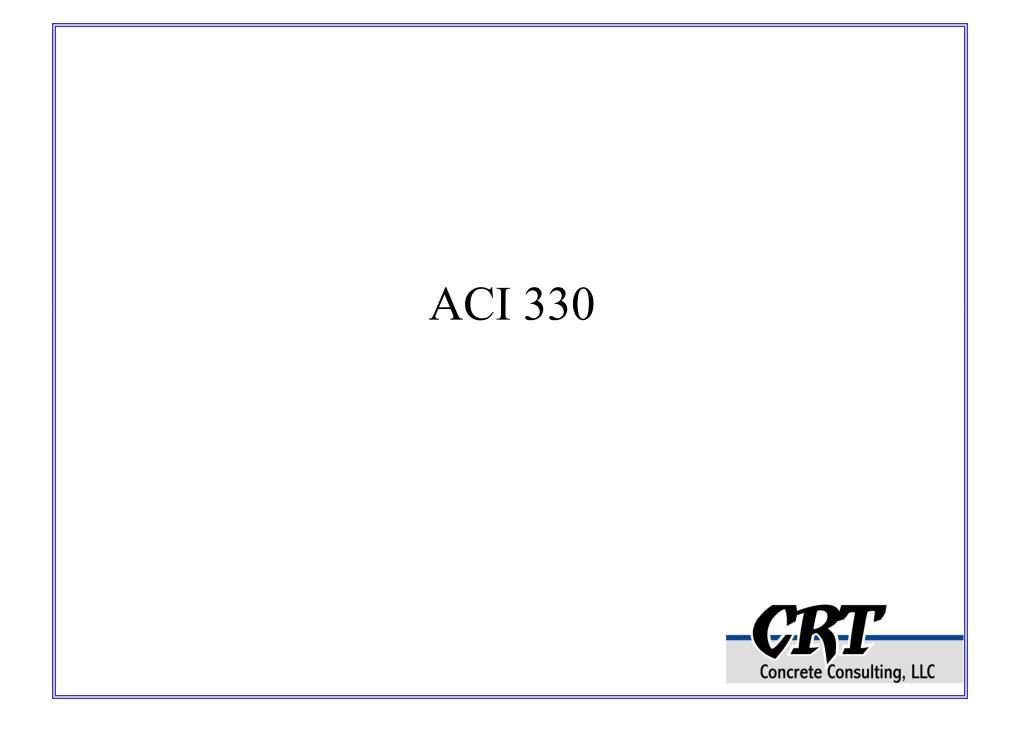
(3-1)





SECONDARY STEEL REINFORCEMENT



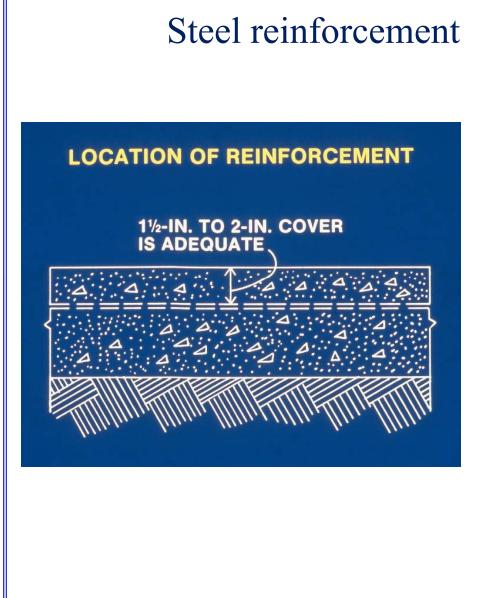


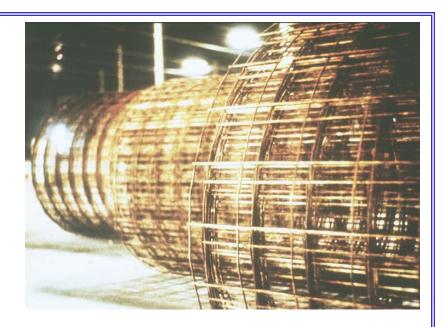
3.81 Distributed Steel Reinforcement

3.8.1 *Distributed steel reinforcement*—When pavement is jointed to form short panel lengths that will minimize intermediate cracking, distributed steel reinforcement is not necessary. The practice of adding distributed steel to

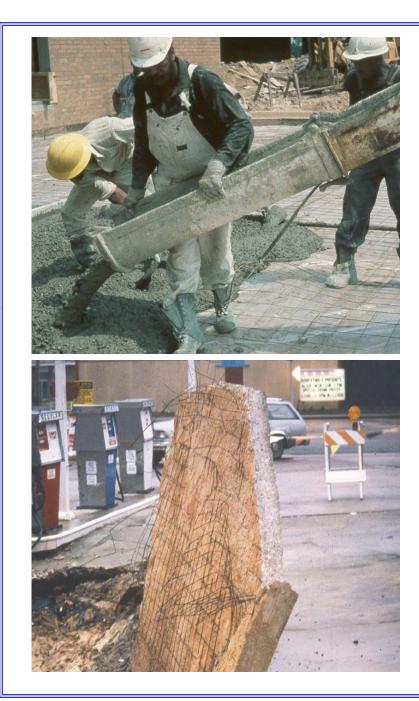
The use of distributed steel reinforcement will not add to the load-carrying capacity of the pavement and should not be used in anticipation of poor construction practices.

joints. The sole function of the distributed steel reinforcement is to hold together the fracture faces if cracks form. The Concrete Consulting, LLC







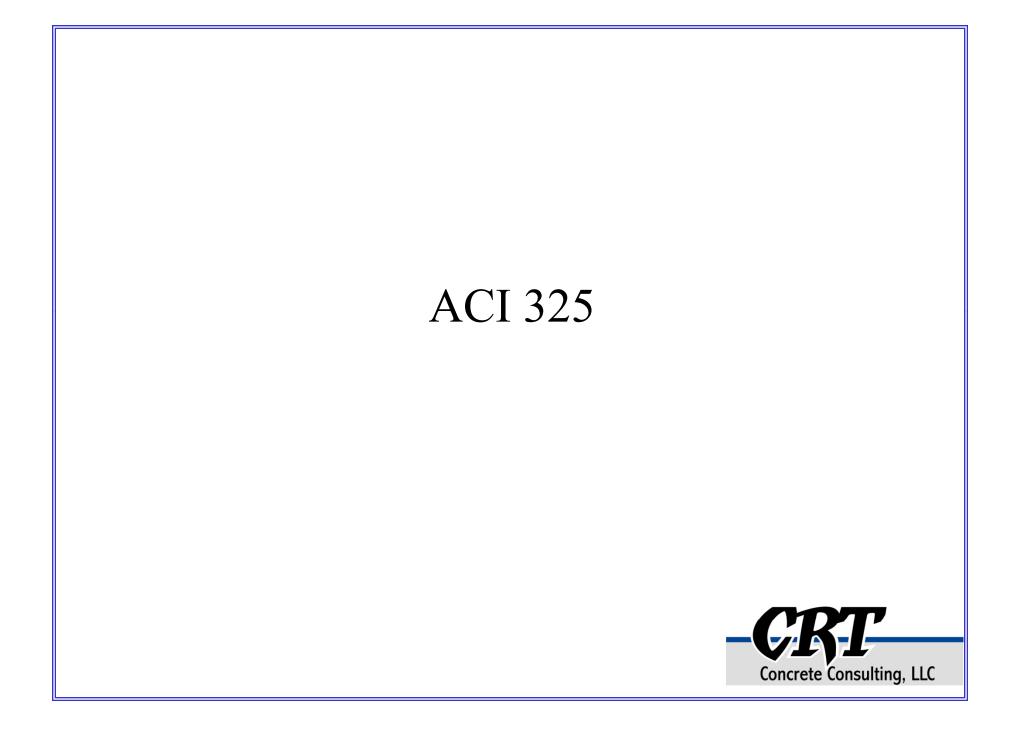


Steel reinforcement

It is almost impossible to place rolled wire mesh in the upper thickness where it can function. Rebar on chairs or welded rigid mats perform better if steel is called for.

Secondary steel reinforcement is often misunderstood and can rarely be justified in flatwork that is properly jointed.

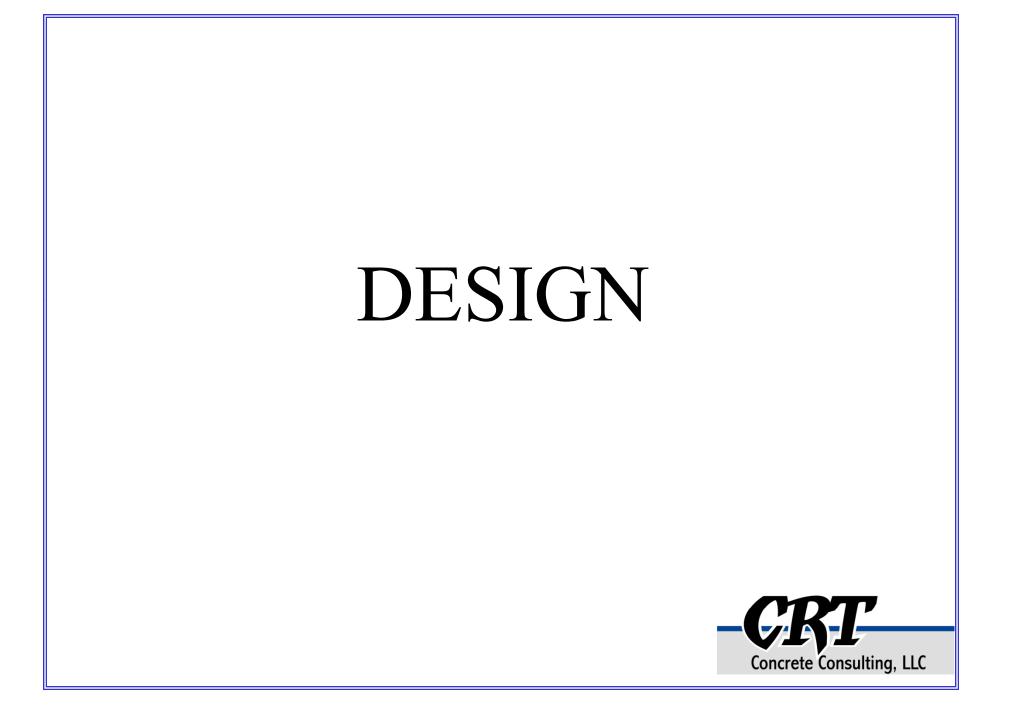




ACI 325 Paragraph 2.2.5

The use of reinforcement is only recommended for lowvolume applications on a limited basis. These limited cases occur when irregular panel shapes are used or when joint spacings are in excess of those that will effectively control shrinkage cracking. Although reinforcing steel cannot be used to address cracking caused by nonuniform support conditions, distributed reinforcement steel may be included to control the opening of unavoidable cracks. The sole function of the steel is to hold together the fracture faces if cracks should form. The quantity of steel varies depending on joint spacing, slab thickness, coefficient of subgrade resistance, bar size, and the tensile strength of the steel. Refer to Chapter 4 for further details of pavement reinforcement design.





ACI 330R thickness table (pg. 7, table 3.4)

Table 3.4—Twenty-year design thickness recommendations, in. (no dowels)

		<i>k</i> = 50	0 psi/in, (C	BR = 50;	R = 86)	k = 400) psi/in. (C	BR = 38; 1	R = 80)	<i>k</i> = 30	0 psi/in. (C	CBR =26; /	R = 67)
	MOR, psi:	650	600	550	500	650	600	550	500	650	600	550	500
Traffic category*	A (ADTT =1)	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.5
	A(ADTT = 10)	4.0	4.0	4.0	4.5	4.0	4.0	4.5	4.5	4.0	4.5	4.5	4.5
	B (ADTT = 25)	4.0	4.5	4.5	5.0	4.5	4.5	5.0	5.5	4.5	4.5	5.0	5,5
	B (ADTT = 300)	5.0	5.0	5,5	5,5	5.0	5.0	5,5	5.5	5.0	5,5	5.5	6.0
	C (ADTT = 100)	5.0	5.0	5,5	5,5	5.0	5.5	5,5	6.0	5,5	5,5	6.0	6.0
	C (ADTT = 300)	5.0	5.5	5,5	6.0	5.5	5.5	6.0	6.0	5.5	6.0	6.0	6.5
	C (ADTT = 700)	5,5	5.5	6.0	6.0	5.5	5.5	6.0	6.5	5,5	6.0	6.5	6.5
Γ	$D (ADTT = 700)^{\dagger}$	6,5	6.5	6.5	6,5	6.5	6.5	6.5	6.5	6.5	6.5	6.5	6.5
MOR, psi:		<i>k</i> = 200 psi/in. (CBR = 10; <i>R</i> = 48)			k = 100 psi/in. (CBR = 3; $R = 18$)				k = 50 psi/in. (CBR = 2; R = 5)				
		650	600	550	500	650	600	550	500	650	600	550	500
	A (ADTT =1)	4.0	4.0	4.0	4.5	4.0	4.5	4.5	5.0	4.5	5.0	5.0	5,5
	A(ADTT = 10)	4.5	4.5	5.0	5.0	4.5	5.0	5.0	5.5	5.0	5,5	5.5	6.0
	B (ADTT = 25)	5.0	5.0	5,5	6.0	5.5	5.5	6.0	6.0	6.0	6.0	6.5	7.0
Traffic	B (ADTT = 300)	5,5	5.5	6.0	6.5	6.0	6.0	6.5	7.0	6.5	7.0	7.0	7.5
category*	C (ADTT = 100)	5,5	6.0	6.0	6.5	6.0	6.5	6.5	7.0	6.5	7.0	7.5	7.5
	C (ADTT = 300)	6.0	6.0	6.5	6.5	6.5	6.5	7.0	7.5	7.0	7.5	7.5	8.0
	C (ADTT = 700)	6.0	6.5	6.5	7.0	6.5	7.0	7.0	7.5	7.0	7.5	8.0	8.5
	$D(ADTT = 700)^{\dagger}$	7.0	7.0	7.0	7.0	8.0	8.0	8.0	8.0	9.0	9.0	9.0	9.0

*ADTT = average daily truck traffic. Trucks are defined as vehicles with at least six wheels; excludes panel trucks, pickup trucks, and other four-wheel vehicles. Refer to Appendix A. k = modulus of subgrade reaction; CBR = California bearing ratio; R = resistance value; and MOR = modulus of rupture.

[†]Thickness of Category D (only) can be reduced by 1.0 in. (25 mm) if dowels are used at all transverse joints (that is, joints located perpendicular to direction of traffic). Note: 1 in. = 25.4 mm; 1 psi = 0.0069 MPa; and 1 psi/in. = 0.27 MPa/m.



Select Traffic Category

Table 2.3—Traffic categories*

1. Car parking areas and access lanes—Category A (autos, pickups, and panel trucks only)

2. Truck access lanes—Category A-1

3. Shopping center entrance and service lanes—Category B

4. Bus parking areas, city and school buses Parking area and interior lanes—Category B Entrance and exterior lanes—Category C

5. Truck parking areas-Category B, C, or D

Truck type	Parking areas and interior lanes	Entrance and exterior lanes
Single units (bobtailed trucks)	Category B	Category C
Multiple units (tractor trailer units with one or more trailers)	Category C	Category D

*Select A, A-1, B, C, or D for use with Table 2.4.



Traffic category		$k = \frac{(CBR)}{M}$				k =			$k = 50$ $(CBR = 2)$ M_R			
	650	600	550	500	650	600	550	500	650	600	550	500
A (ADTT=0)	3.5	3.5	3.5	4.0	3.5	3.5	3.5	4.0	4.0	4.0	4.0	4.0
A-1 (ADTT =1)	4.0	4.0	4.5	4.5	4.0	4.5	4.5	5.0	4.5	5.0	5.0	5.5
A-1 (ADTT = 10)	4.5	5.0	5.5	5.5	5.0	5.5	6.0	6.0	5.5	6.0	6.5	7.0
B (ADTT = 25)	4.5	5.0	5.5	6.0	5.0	5.5	6.0	6.5	5.5	6.0	6.5	7.0
B (ADTT = 300)	5.0	5.5	6.0	6.5	5.5	6.0	6.5	7.0	6.5	6.5	7.0	7.5
(ADTT = 100)	5.5	5.5	0.0	0.5	0.0	0.0	6.5	7.0	6.5	7.0	7.5	8.0
C (ADTT = 300)	5.5	6.0	6.5	7.0	6.0	6.5	7.0	7.5	6.5	7.0	7.5	8.0
C (ADTT = 700)	6.0	6.0	6.5	7.0	6.5	6.5	7.0	7.5	7.0	7.5	8.0	8.5
D (ADTT = 700)	7.0	7.0	7.0	7.0	8.0	8.0	8.0	8.0	9.0	9.0	9.0	9.0

*ADTT = average daily truck traffic. Trucks are defined as vehicles with at least six wheels; excludes panel trucks, pickup trucks, and other four-wheel vehicles. See Appendix A. For thickness conversion to SI units, see Appendix E.



Flexural Strength Sensitivity = $\frac{1}{2}$ "

Traffic category	$k = 500$ $\frac{(CBR = 50)}{M_R}$					$k = \frac{(CBR)}{M}$			$k = 300$ $\frac{(CBR = 26)}{M_R}$			
	650	600	550	500	650	600	550	500	650	600	550	500
$A(ADTT=0)^*$	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5	4.0
A-1 $(ADTT = 1)^*$	3.5	3.5	4.0	4.0	3.5	4.0	4.0	4.0	4.0	4.0	4.0	4.5
A-1 (ADTT = 10)	4.0	4.5	4.5	5.0	4.5	4.5	5.0	5.0	4.5	4.5	5.0	5.5
B (ADTT = 25)	4.0	4.5	4.5	5.0	4.5	4.5	5.0	5.5	4.5	4.5	5.0	5.5
B (ADTT = 300)	5.0	5.0	5.0	5.5	5.0	5.0	5.5	6.0	5.0	5.5	5.5	6.0
C (ADTT = 100)	4.5	5.0	5.5	6.0	5.0	5.0	5.5	6.0	5.0	5.5	5.5	6.0
C (ADTT = 300)	5.0	5.5	5.5	6.0	5.0	5.5	6.0	6.0	5.5	5.5	6.0	6.5
C (ADTT = 700)	5.5	5.5	6.0	6.0	5.5	5.5	6.0	6.5	5.5	6.0	6.0	6.5
D(ADTT = 700)	6.5	6.5	6.5	6.5	6.5	6.5	6.5	6.5	6.5	6.5	6.5	6.5
Traffic category	$k = 200$ (CBR = 10) M_R				$\frac{(\text{CBR} = 3)}{M}$				$k = 50$ $(CBR = 2)$ M_R			
	650	600	550	500	650	♦ 600-	550	500	650	600	550	500
A (ADTT= 0)	3.5	3.5	3.5	4.0	5.5	3.5	5.5	4.0	4.0	4.0	4.0	4.0
A-1 (ADTT =1)	4.0	4.0	4.5	4.5	4.0	4.5	4.5	5.0	4.5	5.0	5.0	5.5
A-1 (ADTT = 10)	4.5	5.0	5.5	5.5	5.0	5.5	6.0	6.0	5.5	6.0	6.5	7.0
B (ADTT = 25)	4.5	5.0	5.5	6.0	5.0	5.5	6.0	6.5	5.5	6.0	6.5	7.0
B (ADTT = 300)	5.0	5.5	6.0	6.5	5.5	6.0	6.5	7.0	6.5	6.5	7.0	7.5
C (AOTT = 100)	5.5	5.5	6.0	6.5	6.0	< 6.0	6.5	7.0	6.5	7.0	7.5	8.0
C (AD17 200)	5.5	6.0	6.5	7.0	6.0	6.5	7.0	7.5	6.5	7.0	7.5	8.0
C (ADTT = 700)	6.0	6.0	6.5	7.0	6.5	6.5	7.0	7.5	7.0	7.5	8.0	8.5

Table 2.4—Twenty-year design thickness recommendations, in. (no dowels)

*ADTT = average daily truck traffic. Trucks are defined as vehicles with at least six wheels; excludes panel trucks, pickup trucks, and other four-wheel vehicles. See Appendix A. For thickness conversion to SI units, see Appendix E.



Subgrade Sensitivity = 1"

Traffic category						(CBR	400 = <u>38</u>)		$k = 300$ $(CBR = 26)$ M_R				
	650	600	550	500	650	600	550	500	650	600	550	500	
$A(ADTT=0)^*$	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5	4.0	
A-1 $(ADTT=1)^*$	3.5	3.5	4.0	4.0	3.5	4.0	4.0	4.0	4.0	4.0	4.0	4.5	
A-1 (ADTT = 10)	4.0	4.5	4.5	5.0	4.5	4.5	5.0	5.0	4.5	4.5	5.0	5.5	
B (ADTT = 25)	4.0	4.5	4.5	5.0	4.5	4.5	5.0	5.5	4.5	4.5	5.0	5.5	
B (ADTT = 300)	5.0	5.0	5.0	5.5	5.0	5.0	5.5	6.0	5.0	5.5	5.5	6.0	
C (ADTT = 100)	4.5	5.0	5.5	6.0	5.0	5.0	5.5	6.0	5.0	5.5	5.5	6.0	
C (ADTT = 200)	5.0	5.5	5.5	6.0	5.0	5.5	6.0	6.0	5.5	5.5	6.0	6.5	
C (ADTT = 700)	5.5	5.5	6.0	6.0	5.5	5.5	6.D	6.5	5.5	6.0	6.0	6.5	
D(ADTT = 700)	6.5	6.5	6.5	6.5	6.5	6.5	6.5	6.5	6.5	6.5	6.5	6.5	
Traffic category		(CBR	$\frac{200}{1} = 10$				$\frac{100}{(3-3)}$			$k = \frac{(CBR)}{M}$			
	650	600	550	500	650	600	55 0	500	650	600	550	500	
A(ADTT=0)	3.5	3.5	3.5	4.0	3.5	3.5	5.0	4.0	4.0	4.0	4.0	4.0	
A-1 (ADTT =1)	4.0	4.0	4.5	4.5	4.0	4.5	4.5	5.0	4.5	5.0	5.0	5.5	
A-1 (ADTT = 10)	4.5	5.0	5.5	5.5	5.0	5.5	6.0	6.0	5.5	6.0	6.5	7.0	
B (ADTT = 25)	4.5	5.0	5.5	6.0	5.0	5.5	6.0	6.5	5.5	6.0	6.5	7.0	
B (ADTT = 300)	5.0	5.5	6.0	6.5	5.5	6.0	6.5	7.0	6.5	6.5	7.0	7.5	
C (ADTT = 100)	5.5	5.5	6.0	6.5	6.0	6.0	6.5	7.0	6.5	7.0	7.5	8.0	
C (ADTT 300)	5.5	6.0	6.5	7.0	6.0	6.5	7.0	7.5	6.5	7.0	7.5	8.0	
C (ADTT = 700)	6.0	6.0	6.5	7.0	6.5	6.5	7.0	7.5	7.0	7.5	8.0	8.5	
D (ADTT = 700)	7.0	7.0	7.0	7.0	8.0	8.0	8.0	8.0	9.0	9.0	9.0	9.0	

Table 2.4—Twenty-year design thickness recommendations, in. (no dowels)

*ADTT = average daily truck traffic. Trucks are defined as vehicles with at least six wheels; excludes panel trucks, pickup trucks, and other four-wheel vehicles. See Appendix A. For thickness conversion to SI units, see Appendix E.



Truck Traffic Sensitivity = $1\frac{1}{2}$ "

Traffic category		(CBR	500 = 50) I_R			$k = \frac{(CBR)}{M}$			$k = 300$ $\frac{(CBR = 26)}{M_R}$			
	650	600	550	500	650	600	550	500	650	600	550	500
$A(ADTT=0)^*$	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5	3.5	4.0
A-1 $(ADTT=1)^*$	3.5	3.5	4.0	4.0	3.5	4.0	4.0	4.0	4.0	4.0	4.0	4.5
A-1 (ADTT = 10)	4.0	4.5	4.5	5.0	4.5	4.5	5.0	5.0	4.5	4.5	5.0	5.5
B (ADTT = 25)	4.0	4.5	4.5	5.0	4.5	4.5	5.0	5.5	4.5	4.5	5.0	5.5
B (ADTT = 300)	5.0	5.0	5.0	5.5	5.0	5.0	5.5	6.0	5.0	5.5	5.5	6.0
C (ADTT = 100)	4.5	5.0	5.5	6.0	5.0	5.0	5.5	6.0	5.0	5.5	5.5	6.0
C (ADTT = 300)	5.0	5.5	5.5	6.0	5.0	5.5	6.0	6.0	5.5	5.5	6.0	6.5
C (ADTT = 700)	5.5	5.5	6.0	6.0	5.5	5.5	6.0	6.5	5.5	6.0	6.0	6.5
D (ADTT = 700)	6.5	6.5	6.5	6.5	6.5	6.5	6.5	6.5	6.5	6.5	6.5	6.5
Traffic category		(CBR	$\frac{200}{1} = 10$			(CBR	$\frac{100}{(3-3)}$			$k = \frac{(CBR)}{N}$		
	650	600	550	500	650	600	550	500	650	600	550	500
A(ADTT=0)	3.5	3.5	3.5	4.0	3.5	3.5	5.0	4.0	4.0	4.0	4.0	4.0
A-1 (ADTT =1)	4.0	4.0	4.5	4.5	4.0	4.5	4.5	5.0	4.5	5.0	5.0	5.5
A-1 (ADTT = 10)	4.5	5.0	5.5	5.5	5.0	5.5	6.0	6.0	5.5	6.0	6.5	7.0
B (ADTT = 25)	4.5	5.0	5.5	6.0	5.0	5.5	6.0	6.5	5.5	6.0	6.5	7.0
B (ADTT = 300)	5.0	5.5	6.0	6.5	5.5	6.0	6.5	7.0	6.5	6.5	7.0	7.5
C (ADTT = 100)	5.5	5.5	6.0	6.5	6.0	6.0	6.5	7.0	6.5	7.0	7.5	8.0
C (ADTT 200)	5.5	6.0	6.5	7.0	6.0	6.5	7.0	7.5	6.5	7.0	7.5	8.0
C (ADTT (799)	6.0	6.0	6.5	7.0	6.5	6.5	7.0	7.5	7.0	7.5	8.0	8.5
D(DTT = 700)	7.0	7.0	7.0	7.0	8.0	8.0	8.0	8.0	9.0	9.0	9.0	9.0

Table 2.4—Twenty-year design thickness recommendations, in. (no dowels)

*ADTT = average daily truck traffic. Trucks are defined as vehicles with at least six wheels; excludes panel trucks, pickup trucks, and other four-wheel vehicles. See Appendix A. For thickness conversion to SI units, see Appendix E.



Parking Area Quick Reference From American Concrete Institute Committee 330

Step 1:	Step 2:	Step 3:	Step 4:	Step 5:	Example:
Determine concrete compressive strength requirement. For all concrete exposed to freeze-thaw cycling and delicers, use no less than 4000 psi. 4500 is recommended.	Determine Modulus of Subgrade Reactivity, k Use guidelines below.	Determine Traffic Categories (Car parkingarea, entrances, etc.).	Determine Average Daily Truck Traffic (ADTT) on the pavement. It is safe to always assume at least one ADTT.	Read across row that corresponds to your Traffic Category and ADTT to the column that represents your concrete strength and k value.	 Car parking area truck access lane. Traffic Category A, ADTT = 1. Concrete strength of 4500 psi. Soil is sandy gravel with some clay and silt; k value is 130–170; therefore use k = 100. Under area with k = 100, read across row with "Traffic Category A (ADTT = 1)" to column underf 'c = 4500. Thickness necessary for this situation is 4.5.

Modulus of Subgra	de Reac	tivity
Type of Subgrade Soll	k Value	CBR
Fine-grained soils in which silt and clay-sized particles predominate	75 - 120	2.5 - 3.5
Sands and sand-gravel mixtures with moderate amounts of silt and clay	130 = 170	4.5 = 7.5
Sands & sand-gravel mixtures relatively free of plastic fines	180 - 220	8.5 - 12

_									
	Tr	affic Categories							
	Select Category A,								
>	Car Parking Areas & Access Lanes (Autos, pick-ups, and panel trucks only) Category A								
>	Shopping Center Entrance and Service Lanes Category B								
>	City & School Bus Parking Areas:								
	& Racking a	rea and interior lanes.	Category B						
	. Entrance	and exterior lanes.	Category C						
>	Truck Parking	Areas:							
	Parking Areas &	Single-Unit Trucks*	Category B						
	Interior Lanes	Multiple-Unit Trucks**	Category C						
	Entrance & Single-Unit Trucks* Category C								
	Exterior Lanes	Category D							
	* Simple (Ind Tausier	a Contrained Teacher							

Single-Unit Trucks = Bobtailed Trucks

** Nultiple-Unit Trucks = Tractor-trailer units with 1 or more trailers

	Twenty-Year Design Thickness Recommendations in Inches (No Dowels)												
		(k = 500 CBR = 5		5)	(k = 400 CBR = 3	i psi ňn. 8; <i>R</i> =80)	k = 300 psilin. (CBR = 26; R =67)			
	<u>t</u> s	5000	4500	4000	3500	5000	4500	4000	3500	5000	4500	4000	3500
	MOR, psi	650	600	550	500	650	600	550	500	650	600	550	500
2	A (ADTT=1)	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.0	4.5
18	A (ADTT=10)	4.0	4.6	4.0	4.5	4.0	4.0	4.5	4.6	4.0	4.5	4.5	4.5
68	B (ADTT=25)	4.0	4.5	4.5	5.0	4.5	4.5	5.0	5.5	4.5	4.5	5.0	5.5
Category*	B (ADTT=300)	5.0	6.0	6.6	5.5	6.0	6.0	6.6	6.6	5.0	6.6	5.5	6.0
	C (ADTT=100)	6.0	6.0	8.6	6.6	6.0	6.6	6.6	6.0	6.6	6.6	6.0	8.0
Traffic	C (ADTT-300)	5.0	5.5	5.5	6.0	5.5	5.5	6.0	6.0	5.5	6.0	6.0	6.5
F	C (ADTT=700)	6.6	5.5	6.0	6.0	6.6	6.6	6.0	6.5	6.6	6.0	6.5	8.6
	D (ADTT=700)†	6.6	6.5	6.5	6.5	6.6	6.6	6.5	6.5	6.5	6.6	6.5	6.5
			k = 200	besilin.			k = 100	in an a li fina			B = 50	psilin.	
			CBR = 1		3)		(CBR = 3		6			2; R =5)	
	fc	5000			3) 3500	5000			3500	5000			3500
	<u>fic</u> MOR, psi		CBR = 1	0; <i>R</i> =48	-		CBR = 3	; <i>R</i> =18)		5000 650	(CBR =	2; R=5)	
		5000	CBR = 1 4500	0; <i>R</i> =48 4000	3500	5000	CBR = 3 4500	: <i>R</i> =18) 4000	3500		(CBR = 4500	2; R =5) 4000	3500
٥ry^	MOR, psi	5000 650	CBR = 1 4500 600	0; <i>R</i> =48 4000 550	3500 500	5000 650	CBR = 3 4500 600	: <i>R</i> =18) 4000 550	3500 500	650	(CBR = 4500 600	2; R =5) 4000 550	3500 500
tegory*	MOR, psi A (ADTT=1)	5000 650 4.0	CBR = 1 4500 600 4.0	0; R =48 4000 550 4.0	3500 500 4.5	5000 650 4.0	CBR = 3 4500 600 4.5	R =18 4000 550 4.5	3500 500 5.0	650 4.5	(CBR = 4500 600 5.0	2; R =5) 4000 550 5.0	3500 500 5.5
Category*	MOR, psi A (ADTT=1) A (ADTT=10)	5000 650 4.0 4.6	CBR = 1 4500 600 4.0 4.5	0; R =48 4000 550 4.0 5.0	3500 500 4.5 5.0	5000 650 4.0 4.5	CBR = 3 4500 600 4.5 5.0	R =18 4000 550 4.5 5.0	3500 500 5.0 5.5	650 4.5 5.0	(CBR = 4500 600 5.0 6.6	2; R =5) 4000 550 5.0 6.6	3500 500 5.5 6.0
fic Category*	MOR, psi A (ADTT=1) A (ADTT=10) B (ADTT=25)	5000 650 4.0 4.5 5.0	CBR = 1 4500 600 4.0 4.5 5.0	0; R =48 4000 550 4.0 5.0 5.5	3500 500 4.5 5.0 8.0	5000 650 4.0 4.5 5.5	CBR = 3 4500 600 4.5 5.0 5.5	R = 18 4000 550 4.5 5.0 6.0	3500 500 5.0 5.5 8.0	650 4.5 5.0 8.0	(CBR = 4500 600 5.0 6.6 8.0	2; R =5) 4000 550 5.0 6.5 8.5	3500 500 5.5 8.0 7.0
	MOR, psi A (ADTT-1) A (ADTT-10) B (ADTT-26) B (ADTT-300)	5000 650 4.0 4.5 5.5	CBR = 1 4500 600 4.0 4.5 5.5	0; R =48 4000 550 4.0 5.0 5.5 6.0	3500 500 4.5 5.0 6.0 6.5	5000 650 4.0 4.5 5.5 6.0	CBR = 3 4500 600 4.5 6.0 5.5 6.0	R = 18 4000 550 4.5 6.0 6.0 6.5	3500 500 5.0 5.5 8.0 7.0	650 4.5 5.0 8.0 6.5	(CBR = 4500 600 5.0 6.6 8.0 7.0	2; R =5) 4000 550 5.0 6.6 8.6 7.0	3500 500 5.5 8.0 7.0 7.5
Traffic Category*	MOR, psi A (ADTT=1) A (ADTT=10) B (ADTT=25) B (ADTT=300) C (ADTT=100)	5000 650 4.0 4.5 5.0 5.5 5.5	CBR = 1 4500 600 4.0 4.5 5.5 5.5 6.0	0; R =48 4000 550 4.0 5.0 5.5 6.0 6.0	3500 500 4.5 5.0 6.0 6.5 6.5	5000 650 4.0 4.5 5.5 6.0 6.0	CBR = 3 4500 600 4.5 5.0 5.5 6.0 6.5	R = 18 4000 550 4.5 5.0 6.0 6.5 6.5	3500 500 5.0 5.5 6.0 7.0 7.0	650 4.5 5.0 8.0 6.5 8.6	(CBR = 4500 600 5.0 6.6 8.0 7.0 7.0	2; R =5) 4000 550 5.0 6.5 6.5 7.0 7.5	3500 500 5.5 6.0 7.0 7.5 7.5

ADTT = Average Daily Truck Traffic Trucks are defined as vehicles with at least 6 wheels; excludes panel trucks, pickup trucks, and other 4-wheeled vehicles. Refer to Appendix A. k = Modulus of subgrade reaction; CBR = California Bearing Ratio; R = Resistance value; and MOR = Modulus Of Rupture.

† Thickness of Category D (only) can be reduced by 1.0 in. (25 mm) if dowels are used at all transverse joints (that is, joints located perpendicular to direction of traffic). Note: 1 in. = 25.4 mm; 1 psi = 0.0069 MPa; and 1 psi/in. = 0.27 MPa/m.

DESIGN OF JOINTED PAVEMENTS FOR LOCAL STREETS AND ROADS

(ACI 325)



ACI 325.12R-02

Guide for Design of Jointed Concrete Pavements for Streets and Local Roads

Reported by ACI Committee 325

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3.1 of ACI 325

CHAPTER 3—PAVEMENT THICKNESS DESIGN 3.1—Basis of design

The most cost-effective pavement design is that which has been validated by road tests, pavement studies, and surveys of pavement performance. The most commonly used methods are the AASHTO design guide,² which was developed from performance data obtained at the AASHTO road test; and the Portland Cement Association's (PCA) design procedure,^{12,13} which is based on the pavement's resistance to fatigue and deflection effects on the subgrade. The PCA procedure is recommended for use in instances of overload conditions that can yield design thicknesses beyond those provided in this chapter. Further explanations of design concepts suggested in the PCA design procedure can be found in Appendix A. A design catalog published by the National Cooperative Highway Research Program (NCHRP) may also provide useful design information.²⁵



ACI 325

	VPD or ADT,	(two-axle,	ercial vehicles six-tire, and wier)
Street classification	two-way	%	No. per day
Light residential	200	1 to 2	2 to 4
Residential	200 to 1000	1 to 2	2 to 4
Collector	1000 to 8000	3 to 5	50 to 500
Minor arterial	4000 to 15,000	10	300 to 600
Major arterial	4000 to 30,000	15 to 20	700 to 1500
Business	11,000 to 17,000	4 to 7	400 to 700
Industrial	2000 to 4000	15 to 20	300 to 800



3.3 Thickness Determination

- Subgrade Support
- Flexural Strength
- Traffic

3.3—Thickness determination

Proper selection of the slab thickness is a crucial element of a concrete pavement design. Inadequate thickness will lead to cracking and premature loss of serviceability. Suggested thicknesses for the design of low-volume concrete roads are listed in Table 3.2(a) and 3.2(b) as a function of subgrade support and concrete flexural strength (third-point loading). The thicknesses listed for a k value of 81.5 MPa/m (300 psi/in.) are considered to be minimum thicknesses for design. Pavement designs provided in these tables are assumed to be applicable to a 30-year performance period as long as minimal durability-related distresses occur. Pavement life can also be assessed from the standpoint of fatigue accumulation based on calculations illustrated in Appendix A.



ACI 325

		13.3 Mill					- 27 1412				
		MOR MP	1				MOR MP			ł	
.4	3.8	4,1	4.5	4.8	3.4	3.8	4,1	4.5	4.8	Taffi	e classification
50	150	150	125	125	150	125	125	125	125	ADTT = 3	Light residential
75	175	150	150	150	175	150	150	125	125	ADTT = 10	Residential
75	175	150	150	150	175	150	150	125	125	ADTT = 20	
75	175	150	150	150	175	150	150	150	125	ADTT = 50	Collector
00	200	175	175	175	200	175	175	150	150		
25	200	200	175	175	200	175	175	175	150	ADTT = 100	
25	200	200	200	200*	200	200	175	175	175	ADTT = 500	Minor arterial
25	200	200	200	200*	200	200	175	175	175	ADTT = 100	
25	225	200	200*	200†	225	200	175	175	175	ADTT = 500	Major arterial
50	225	225	200	200*	225	225	200	200	175	ADTT = 400	Major aneriai
50	250	225	225*	225	225	225	200	200*	200†	ADTT = 800	
75	250	250	250	2508	250	225	225	225	225	ADTT = 1500	Business
25	200	200	175	175	200	200	175	175	150	ADTT = 300	1
25	225	200	200	200 [†]	200	200	175	175	175	ADTT = 700	Industrial
50	225	225	200	200*	225	225	200	200	175	ADTT = 400	industrial
50	250	225	225*	225	225	225	200	200*	200†	ADTT = 800	_
	k	= 54 MPa	/m			k=	81.5 MPa	ı/m			
		MOR MP					MOR MP				
,4	3.8	4,1	4.5	4.8	3.4	3.8	4,1	4.5	4.8		e classification
25	125	125	100	100	125	125	100	100	100	ADTT = 3	Light residential
50	125	125	125	125	150	125	125	125	100	ADTT = 10	Residential
50	150	125	125	125	150	125	125	125	100	ADTT = 20	
50 75	150	125	125	125	150	125	125	125	125	ADTT = 50	Collector
75	175	150	150	150	175	150	150	150	125	ADTT = 100	
00	175	175	150	150	175	175	150	150	150	ADTT = 500	Minor arterial
00	175	175	150	150	175	175	150	150	150	ADTT = 100	
00	175	175	175	175	175	175	175	175	175	ADTT = 500	
00	200	175	175	175	200	175	175	175	175	ADTT = 400	Major arterial
25	200	200	175	175	200	200	175	175	175	ADTT = 800	
25	200	200	200*	200 [†]	200	200	200*	200*	200	ADTT = 1500	Business
75	175	175	150	150	175	175	150	150	150	ADTT = 300	
00	175	175	175	175	175	175	150	150	150	ADTT = 700	
00	200	175	175	175	200	175	175	175	175	ADTT = 400	Industrial

Note: 1 in. = 25.4 mm; and 1 pti/in. = 0.27 MPa/m.

*If doweled, thickness can be decreased by 13 mm. [†]If doweled, thickness can be decreased by 25 mm.

⁴If doweled, thickness can be decreased by 38 mm. ⁸If doweled, thickness can be decreased by 50 mm.



		avenie .	in the second	0 01 011		oported edges)					
		MORING					MORMP				
3.4	3.8	MOR MPa 4.1	4.5	4.8	3.4	3.8	4.1	4.5	4.8	Traffic	classification
175	175	150	150	150	175	150	150	150	125	ADTT = 3	Light residential
200	200	175	175	150	175	175	175	150	150	ADTT = 10	Residential
200	200	200	175	175	200	175	175	150	150	ADTT = 20	
200	200	200	175	175	200	175	175	175	150	ADTT = 50	Collector
250	225	225	200	200	225	200	200	175	175	ADTT = 50	
250	225	225	200	200	225	200	200	200	175	ADTT = 100	
275	250	225	225	200	250	225	200	200	200	ADTT = 500	Minor arterial
275	250	225	225	200	250	225	200	200	200	ADTT = 100	1
275	250	250	225*	225*	250	225	225	200	200*	ADTT = 500	Majorarterial
300	275	250	250	225	275	250	225	225	200	ADTT = 400	wajer arteriar
300	275	275	250*	250	275	250	250	225	225*	ADTT = 800	
300	300	275	275	275	275	250	250	250	250	ADTT = 1500	Business
250	250	225	225	200	225	225	200	200	175	ADTT = 300	
275	250	225	225	225*	250	225	225	200	200	ADTT = 700	Industrial
300	275	250	250	225	275	250	225	225	200	ADTT = 400	and the second second
300	300	275	250	250	275	250	250	225	225	ADTT = 800	-
	k	= 54 M Pa/	im			<i>k</i> •	81.5 MPa	/m			
		MOR MP					MOR M Pa				
3.4	3.8	4,1	4.5	4.8	3.4	3.8	4,1	4.5	4.8		elassification
150	150	125	125	125	150	125	125	125	125	ADTT = 3	Light residential
175	150	150	150	125	150	150	150	125	125	ADTT = 10	Residential
175	175	150	150	150	175	150	150	150	125	ADTT = 20	
175	175	150	150	150	175	150	150	150	125	ADTT = 50	Collector
200	200	175	175	150	200	175	175	150	150	ADTT = 50	
200	200	175	175	175	200	175	175	150	150	ADTT = 100	
225	200	200	175	175	200	200	175	175	175	ADTT = 500	Minor arterial
225	200	200	175	175	200	200	175	175	175	ADTT = 100	
225	200	200	200	200	225	200	200	175	175	ADTT = 500	Majorarterial
250	225	225	200	200	225	225	200	200	175	ADTT = 400	-
250	225	225	200	200*	225	225	200	200	200	ADTT = 800	
250	225	225	225*	225*	250	225	225	225*	225†	ADTT = 1500	Business
225	200	200	175	175	200	200	175	175	175	ADTT = 300	
225	200	200	175	175	200	200	175	175	175	ADTT = 700	Industrial
250	225	225	200	200	225	225	200	200	175	ADTT = 400	
250	225	225	200	200*	225	225	200	200	200	ADTT = 800	_

Table 3.2(b)—Pavement thickness, mm,²⁹ without curb and gutters or shoulders (unsupported edges)

Note: 1 in. = 25.4 mm; and 1 psi/in. = 0.27 MPa/m.

If doweled, thickness can be decreased by 13 mm. If doweled, thickness can be decreased by 25 mm.



Pavement Thickness with Integral or Tied Curb & Gutter or Shoulders

	k= 100 psi/in											'in	= 50 psi/i	k		
						MOR psi						i	MOR psi			
Classification	Traffic	0	70	0	65	600	550	500)	700	50		600)	550	500
Light Residential	ADTT = 3		5		5	5	5	6		5	5		6		6	6
Residential	ADTT = 10		5		5	6	6	7		6	5	Т	6		7	7
	ADTT = 20		5		5	6	6	7		6	5	Τ	6		7	7
Collector	ADTT FO		5		6	6	6	7		6	5	Τ	6		7	7
	ADTT = 50		6		6	7	7	8		7	7	Τ	7		8	8
	ADTT = 100		6		7	7	7	8		7	7	Τ	8		8	9
Minor Arterial	ADTT = 500		7		7	7	8	8	*	8	3	Τ	8		8	9
	ADTT = 100		7		7	7	8	8	*	8	3	Τ	8		8	9
Maine Antonial	ADTT = 500	*	7		7	7	8	9	+	8	3*	╈	8		9	9
Major Arterial	ADTT = 400		7	_	8	8	9	9	*	8	3	\top	9		9	10
	ADTT = 800	+	8	*	8	8	9	9	+	9) *	Τ	9		10	10
Business	AD 11 - 1500	*	9	*	9	9 *	9	10	ş	10	0 ‡	ŀ	10 +	*	10	11
	ADTT = 300		6		7	7	8	8		7	7	Τ	8		8	9
In december 1	ADTT = 700	*	7	*	7	7	8	8	+	8	3*	\top	8		9	9
Industrial	ADTT = 400		7		8	8	9	9	*	8	3	\top	9		9	10
-	ADTT = 800	†	8	*	8	8	9	9	+	9) *		9		10	10
					-							-	-	_		

* If doweled, thickness can be decreased by 0.5 in

† If doweled, thickness can be decreased by 1 in

‡ If doweled, thickness can be decreased by 1.5 in

§ If doweled, thickness can be decreased by 2 in



3.7: JOINTING



Joint layout guidelines

- Things to Do
 - Jointing plan drawn by designer of record, or submitted by contractor & approved by designer
 - Match existing joints or cracks
 - Cut at the proper time
 - Place joints to meet in-pavement structures
 - Adjust spacings to avoid small panels or angles
 - Intersect curves radially, edges perpendicular
 - Keep panels square

- Things to Avoid
 - Jointing plan left to contractor with no oversight
 - Slabs < 1 ft. wide
 - Slabs > 15 ft. wide
 - Angles $< 60^{\circ}$ (90° is best)
 - Creating interior corners
 - Odd Shapes (keep slabs square)
 - Offset (staggered) joints
 - Isolation (unthickened) joints in traffic areas



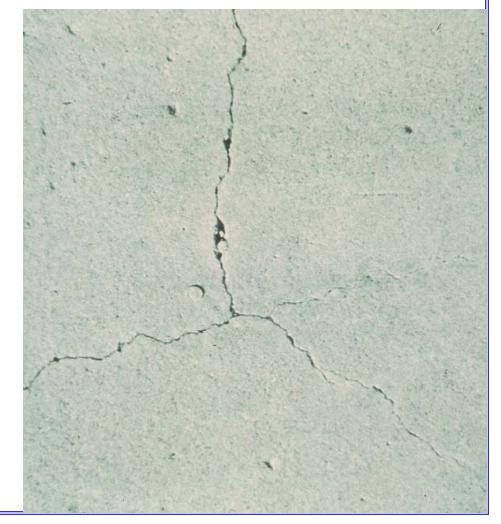
Joint design and layout affects performance...

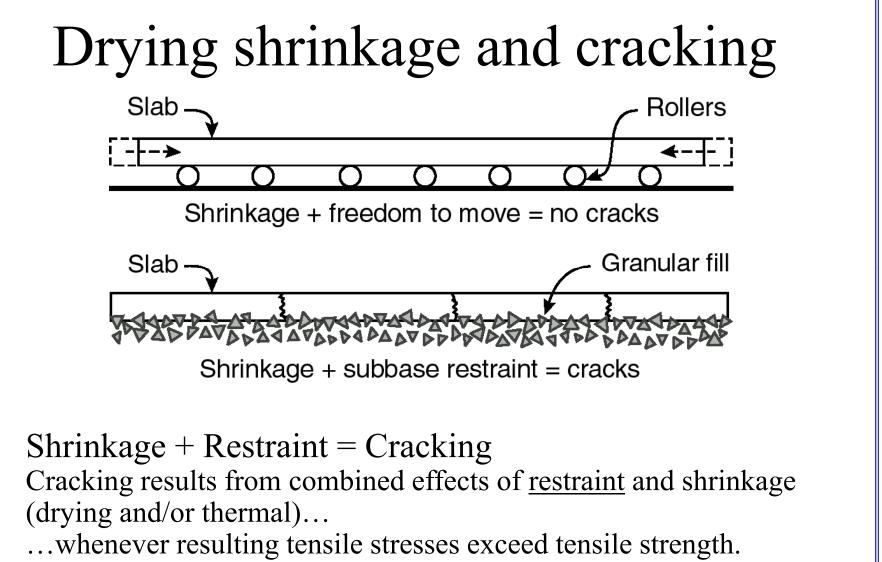


Concrete volume change effects and jointing

Concrete volume change (and cracking) behavior is the basis of many jointing and construction procedure recommendations.

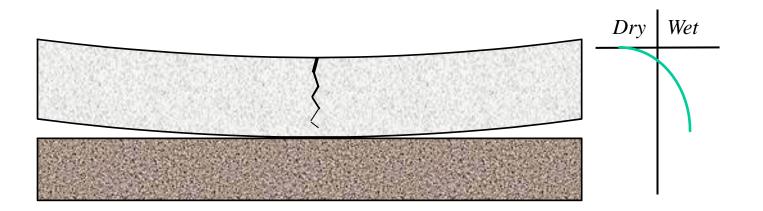








Differential shrinkage = warping or curling of slabs



- Can result from differential moisture created by surface drying while the slab bottom remains wet
- Can also result from differential temperature
- Effects become more severe with thinner slabs and/or longer joint spacings
- In severe cases, causes loss of support near panel edges, greater movement and faulting at joints, mid-panel cracking

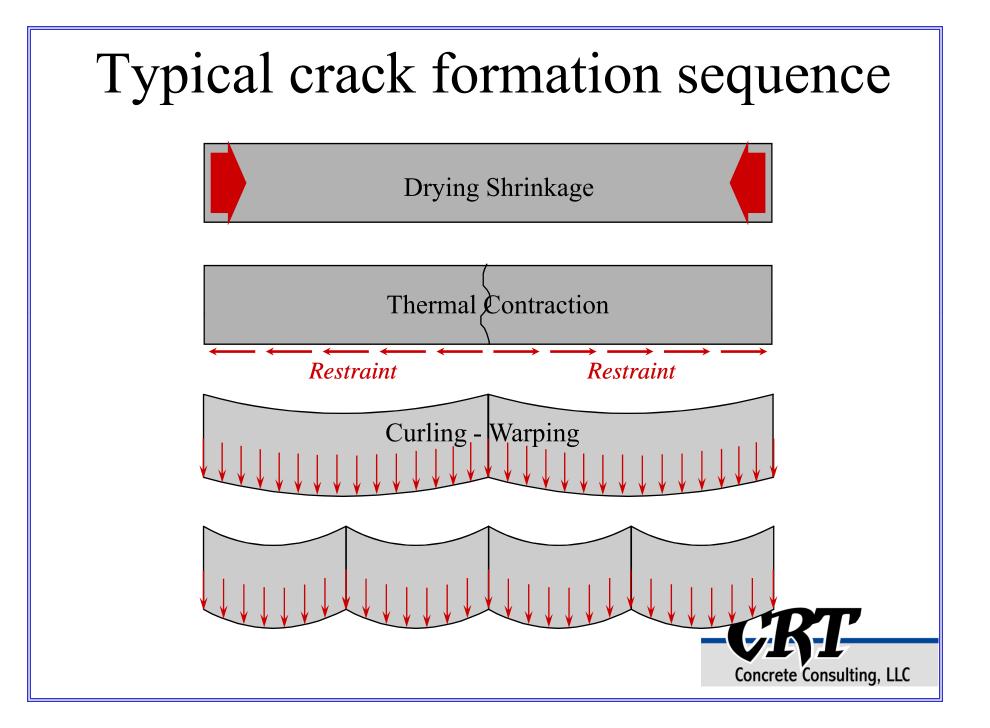


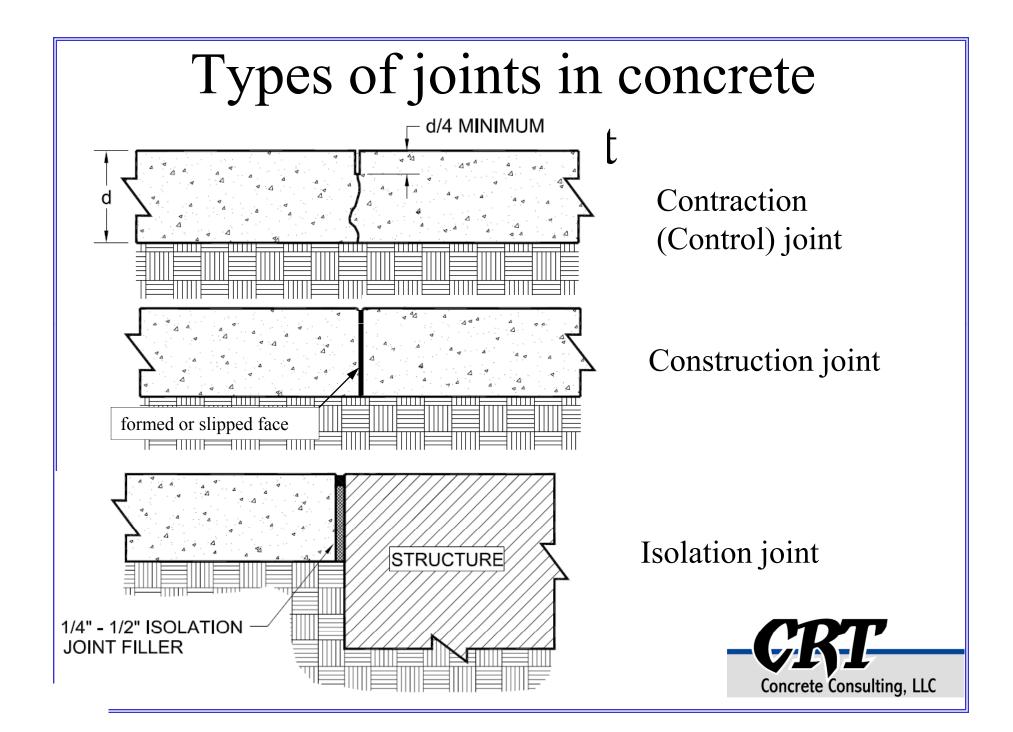
Objectives of jointing



- Control the location, width, and appearance of expected cracks
- Facilitate construction
- Accommodate normal slab movements
- Provide load transfer where needed
- Minimize performance implications of any random (unexpected) cracks

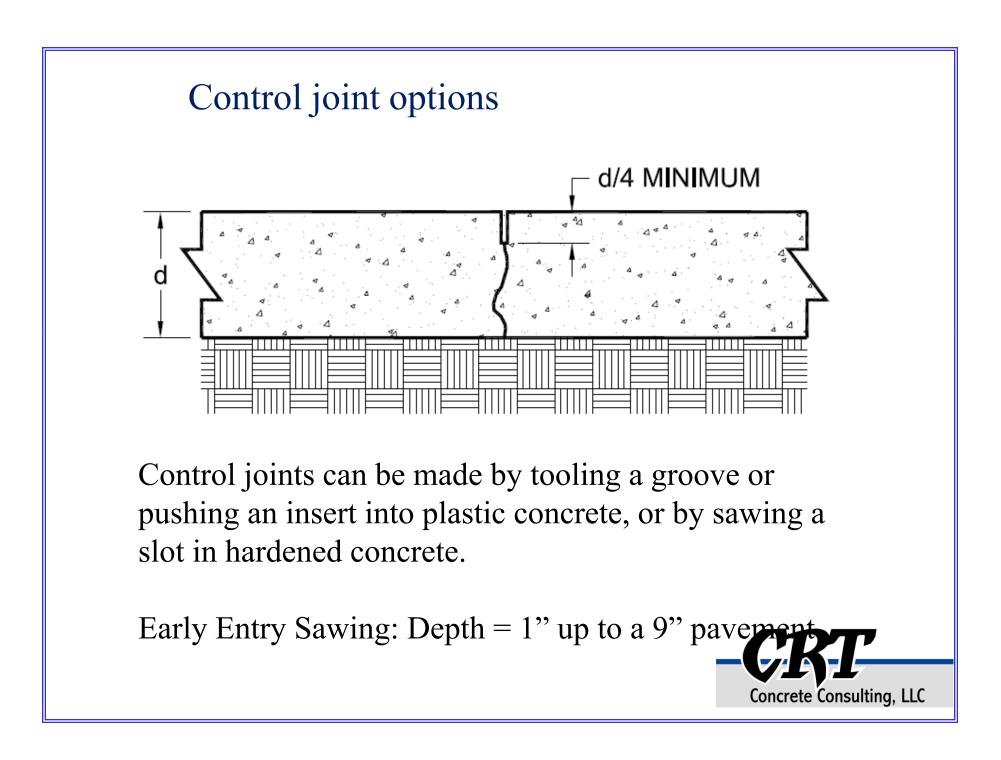






3.7.1: CONTRACTION (CONTROL) JOINTS





Three Rules of Thumb for Control Joints.

- Spacing: Maximum of 2.5 times the depth in feet
 - 4" thick: 10' max (4 x 2.5)
 - Maximum 15' on center
- Depth: Minimum of ¼ of the depth: 8" thick = 2" deep
 - Early Entry may apply
- Panel shall be kept as square as possible
 - 1.5:1



Spacing of joints based on cracking tendency

The extent of cracking due to key influences is somewhat predictable; joints can be spaced accordingly.



RECOMMENDED SPACING of JOINTS FOR CRACK CONTROL

Table 3.5—Spacing between joints

Pavement thickness, in. (mm)	Maximum spacing, ft (m)
4, 4.5 (100, 113)	10 (3.0)
5, 5.5 (125, 140)	12.5 (3.8)
6 or greater (150 or greater)	15 (4.5)

Exception: good design may call for even closer joint spacings due to load transfer considerations.





Tooled control joints

Advantages:

- Simplest to make
- Most reliable crack initiation

Disadvantages:

- Most noticeable joint
- Not smoothest for rolling wheels
- Not designed for sealers / fillers

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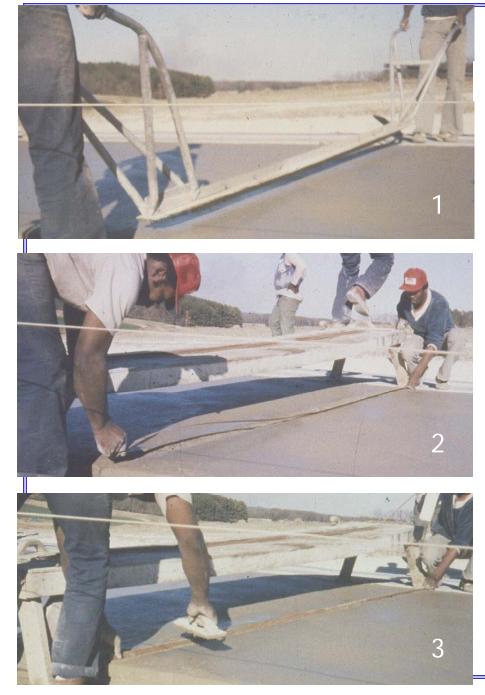
Insert control joints



Advantages:

- Almost invisible
- Somewhat resistant to intrusion of water and debris even when left unsealed
- Provides good rideability
- Reliable crack initiation
- Fast and economical <u>Disadvantage</u>s:
- Learning curve for crew
- Can ravel or spall if not installed plumb





Insert joint construction sequence





Spalling results if the insert is not plumb.



Plastic strip insert joint after 12 years of service



Sawcut control joints



Advantages:

- Makes best sealant reservoir
- Not as noticeable as tooled
- Smoothest for wheels

Disadvantages:

- Timing is critical to success least reliable crack initiation with gravel aggregates
- Expensive to make



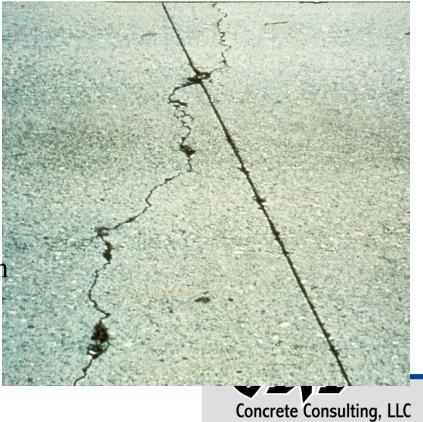
Timing of joint sawing – a critical factor

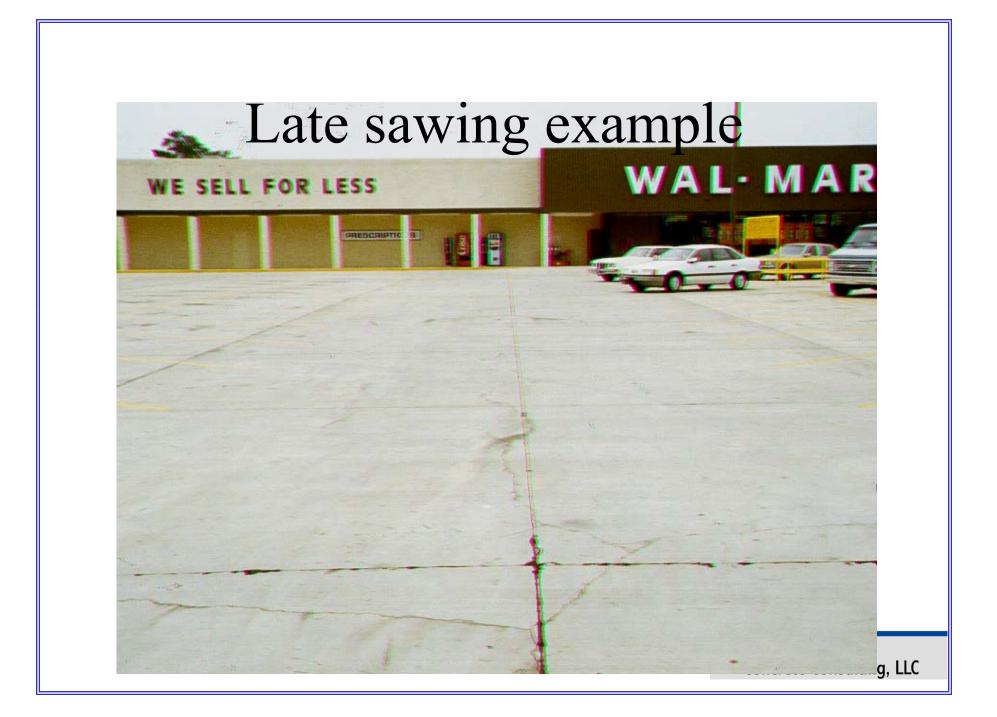


 \clubsuit This joint was sawedsoon enough

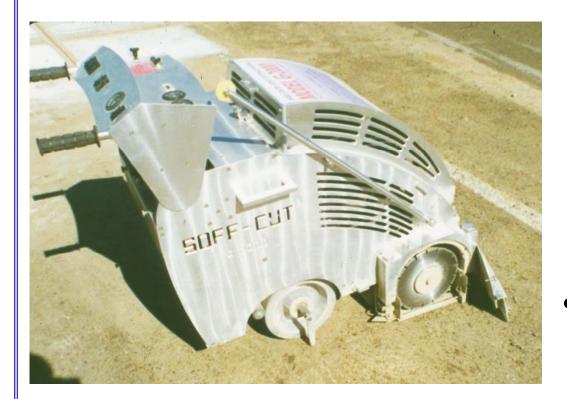
This one was sawed too late \rightarrow

Sawcut joints must be made within 4-12 hours after final finishing

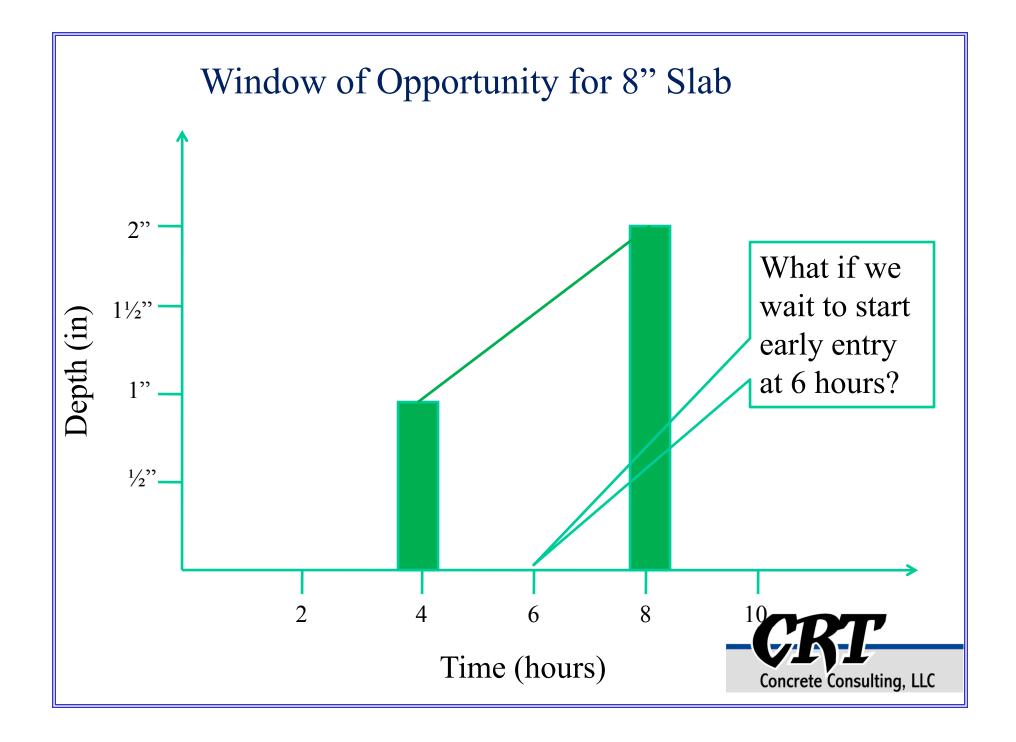




Early entry "dry cut" saws



- Designed to initiate cracks with a shallow cut made much earlier than with wet-cut saws
- Timing the "window of opportunity" is 1 to 2 hopportunity



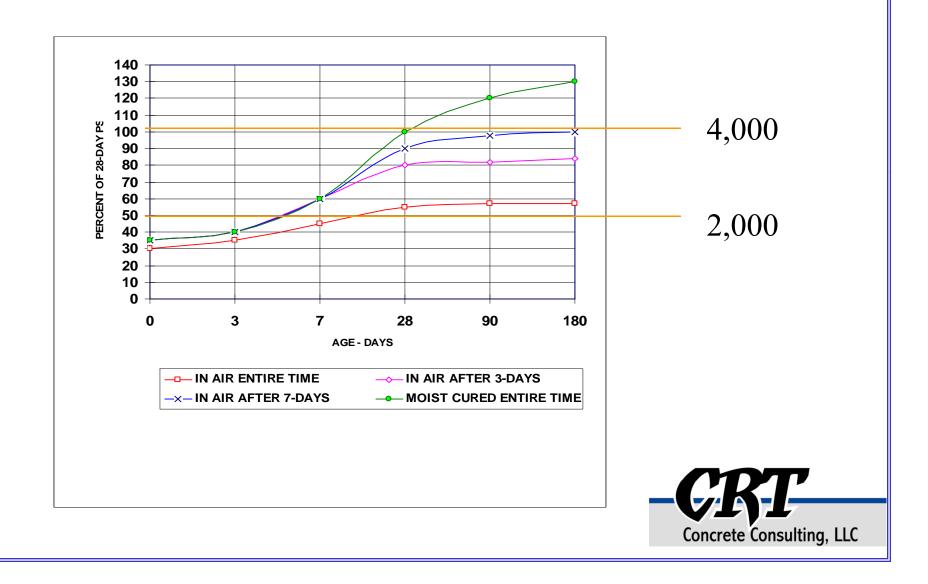


CURING

- TIME to develop strength
- TEMPERATURE to drive chemistry
- MOISTURE for hydration



Moisture is Required....



Curing

- Spray membrane curing compound - ASTM C 309, white pigmented preferred
- Timing is critical spray immediately after finishing
- Suggested application rate:
 - Maximum coverage: 200 ft²/ gal
 - Higher rate (less coverage) for windy or dry conditions





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QUESTIONS?

